



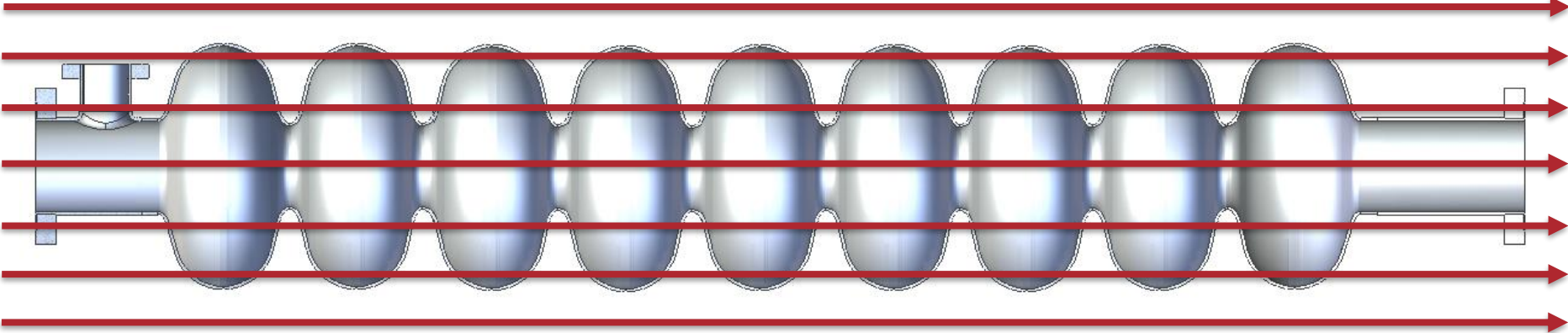
# Magnetic Flux Expulsion Studies on Niobium

Sam Posen & Fermilab SRF Team  
SRF Conference 2017  
18 July 2017

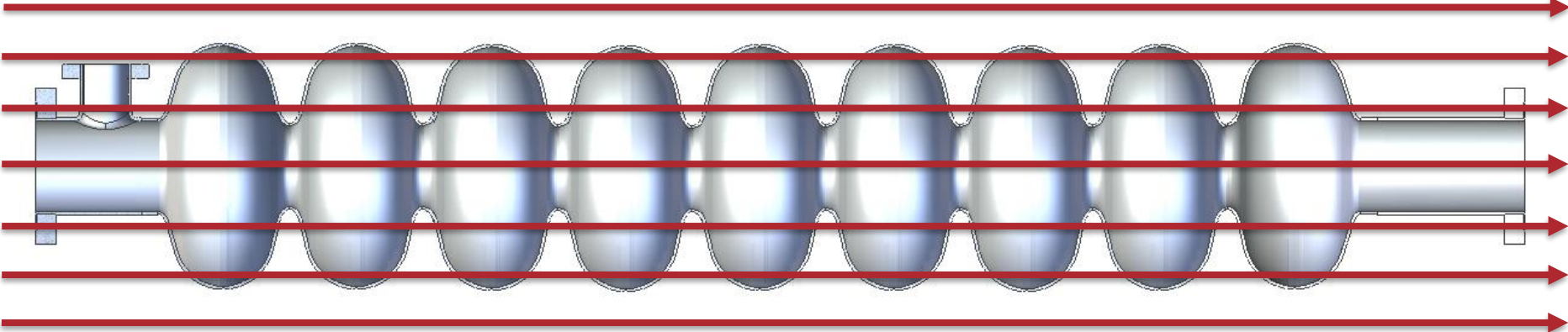


Live from Batavia, USA!

# Why Flux Expulsion is Important

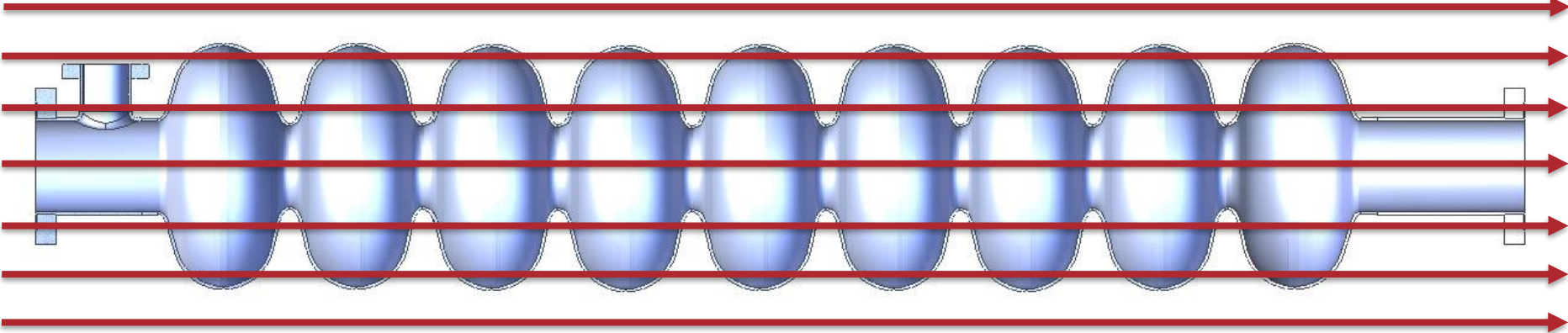


LCLS-II CAV0007 – fabricated and prepared by RI, TD material

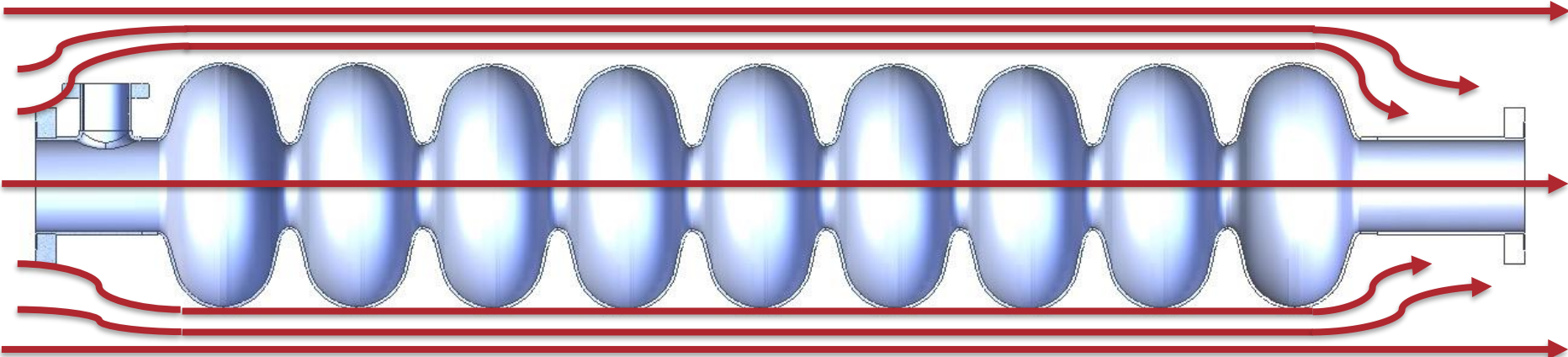


LCLS-II CAV0019 – fabricated and prepared by RI, TD material

# Why Flux Expulsion is Important



LCLS-II CAV0007 – fabricated and prepared by vendor B, TD material



LCLS-II CAV0019 – fabricated and prepared by vendor B, TD material

# Why Flux Expulsion is Important

Cavity	Usable Gradient* [MV/m]	Q0 @ 16 MV/m (or useable gradient) 2 K
CAV0008	20.5	2.0E+10
CAV0003	21.0	2.5E+10
CAV0006	21.0	2.0E+10
CAV0007	21.0	2.2E+10
CAV0016	18.2	1.8E+10
CAV0013	16.5	2.0E+10
CAV0011	20.5	2.3E+10
CAV0015	21.0	2.3E+10
<b>Average</b>	<b>20.0</b>	<b>2.1E+10</b>
<b>Total Voltage</b>	<b>166 MV</b>	

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CAV0027	21.0	3.2E+10
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CAV0042	16.8	2.8E+10
CAV0032	21.0	3.0E+10
<b>Average</b>	<b>17.6</b>	<b>3.5E+10</b>
<b>Total Voltage</b>	<b>146 MV</b>	

Fermilab CM-2  
Cavities treated with  
baseline recipe

Fermilab CM-3  
Treatment modified to  
improve flux expulsion

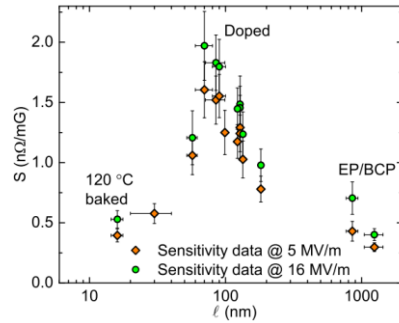
Total voltage Spec: 133 MV      Q<sub>0</sub> Spec: 2.7x10<sup>10</sup>

Magnetic Flux Expulsion  
**Background**

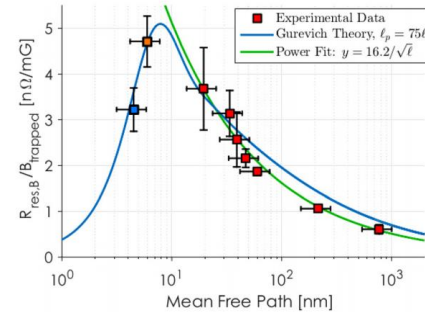


# Expulsion is an Important Factor in Flux Losses

- Determines what fraction of ambient flux becomes trapped
- Other factors:
  - Sensitivity to trapped flux

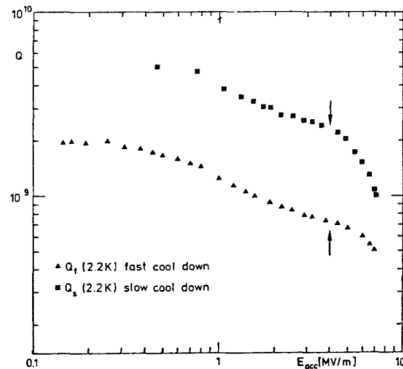


M. Martinello et al.  
Appl. Phys. Lett.  
109, 062601 (2016)

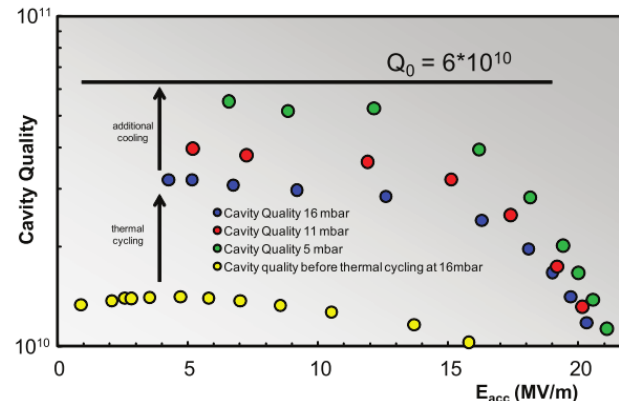


D. Gonnella et al.  
Appl. Phys. Lett.  
119, 073904 (2016)

- Thermocurrents due to connections near cavity (e.g. He vessel)
- Thermocurrents due to bilayers (e.g. Nb<sub>3</sub>Sn/Nb)



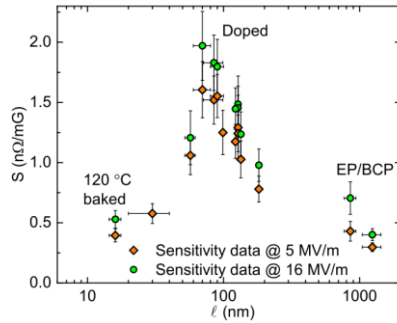
M. Peiniger et al.  
SRF Workshop  
(1988).



O. Kugeler et al.  
SRF Conference  
(2009).

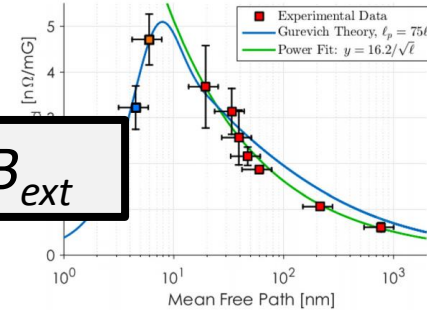
# Expulsion is an Important Factor in Flux Losses

- Determines what fraction of ambient flux becomes trapped
- Other factors:
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M. Martinello et al.  
Appl. Phys. Lett.  
109, 062201 (2016)

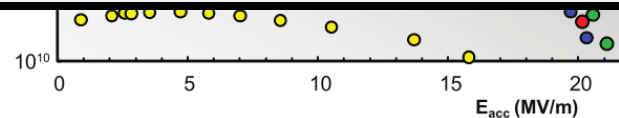
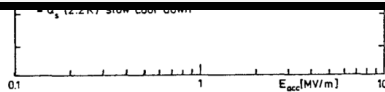
$$R_{fl} = S \cdot \eta \cdot B_{ext}$$



D. Gonnella et al.  
Appl. Phys. Lett.  
119, 073904 (2016)

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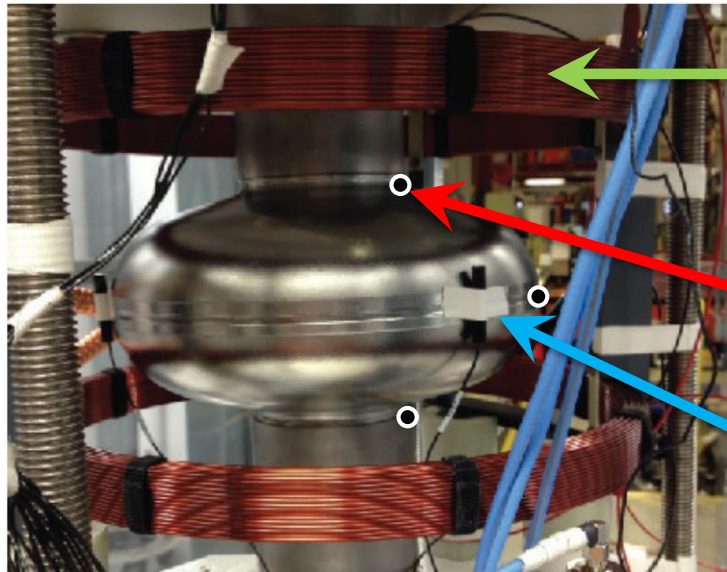
$S$  depends on surface treatment (e.g. N-doping vs EP)  
 $B_{ext}$  depends on shielding, hygiene, thermocurrents  
 What about  $\eta$ ? Recent experimental evidence: thermal gradient during cooldown & **bulk structure**



et al.  
reference

## Measuring Flux Expulsion

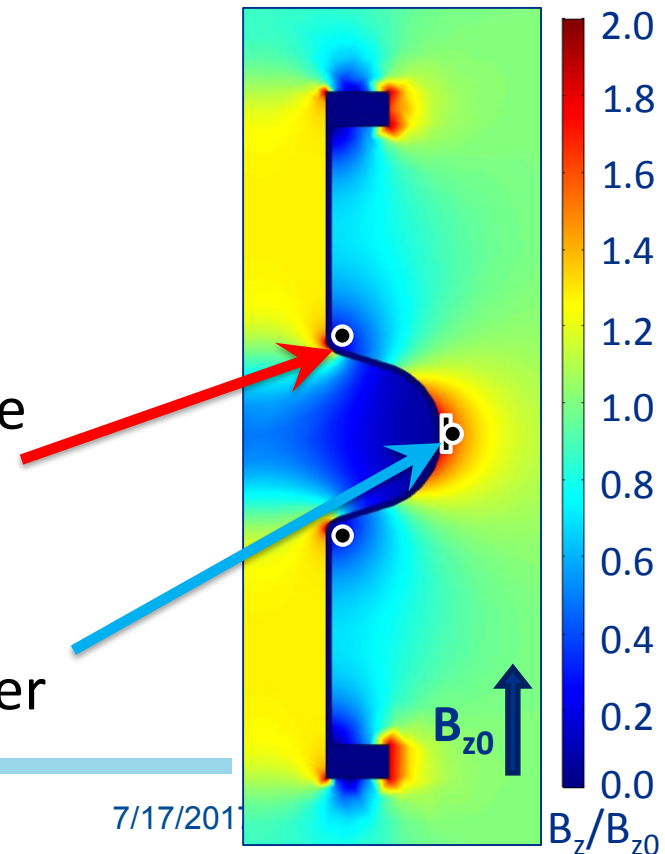
- An axial magnetic field is applied during cooldown. Fluxgate magnetometers at the equator measured the magnetic field before  $B_{NC}$  and after  $B_{SC}$  superconducting transition.
  - Complete trapping:  $B_{SC}/B_{NC} = 1$
  - Complete expulsion:  $B_{SC}/B_{NC} \sim 1.7$



External field coils

Temperature sensor

Fluxgate magnetometer



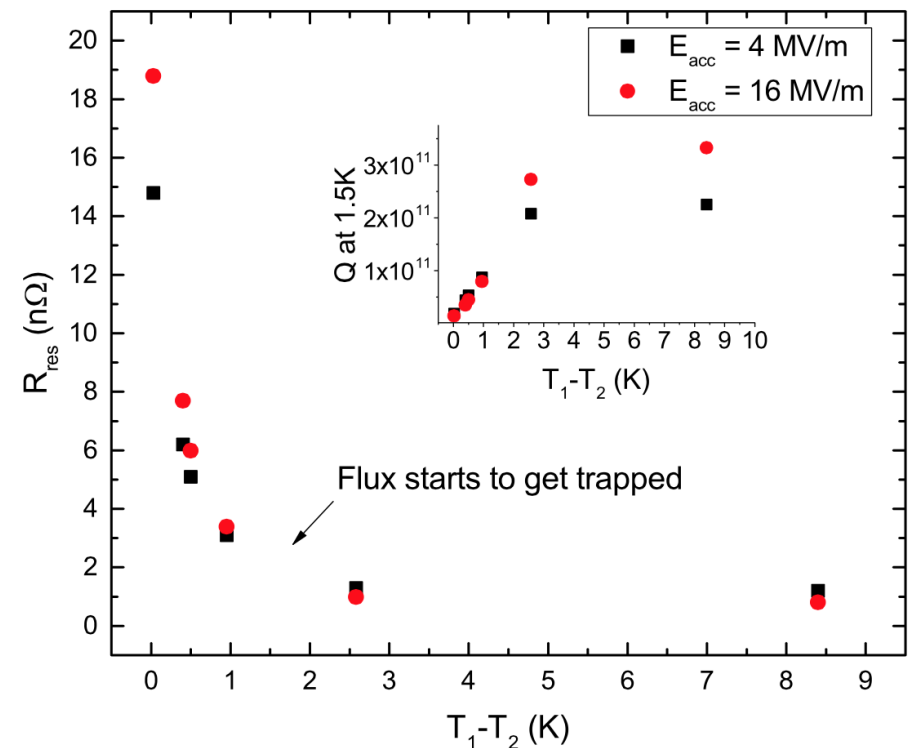
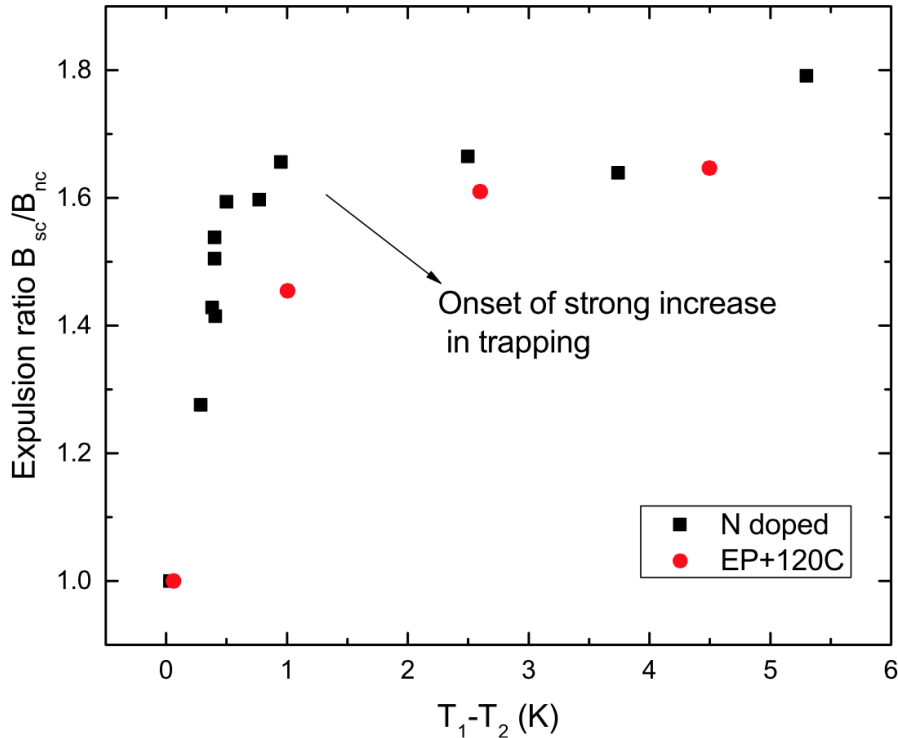
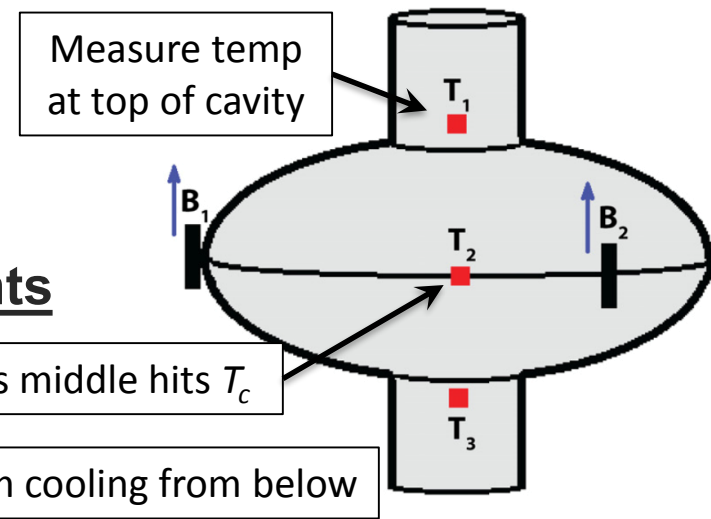


Magnetic Flux Expulsion

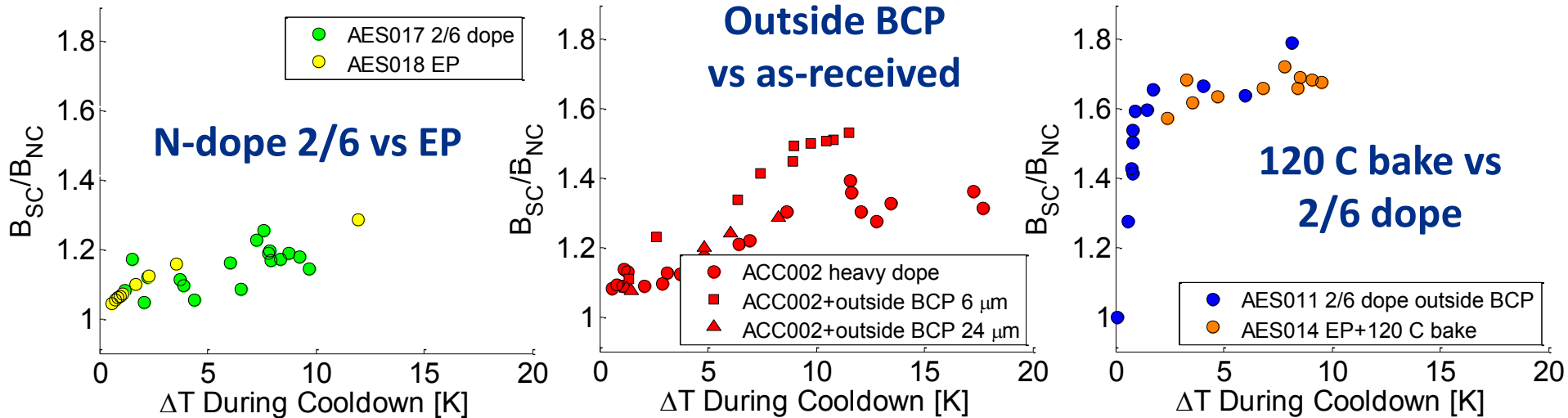
**Results of Experiments to Probe  
the Physics of Flux Expulsion**

# 1) Large thermal gradients at $T_c$ promote expulsion of flux

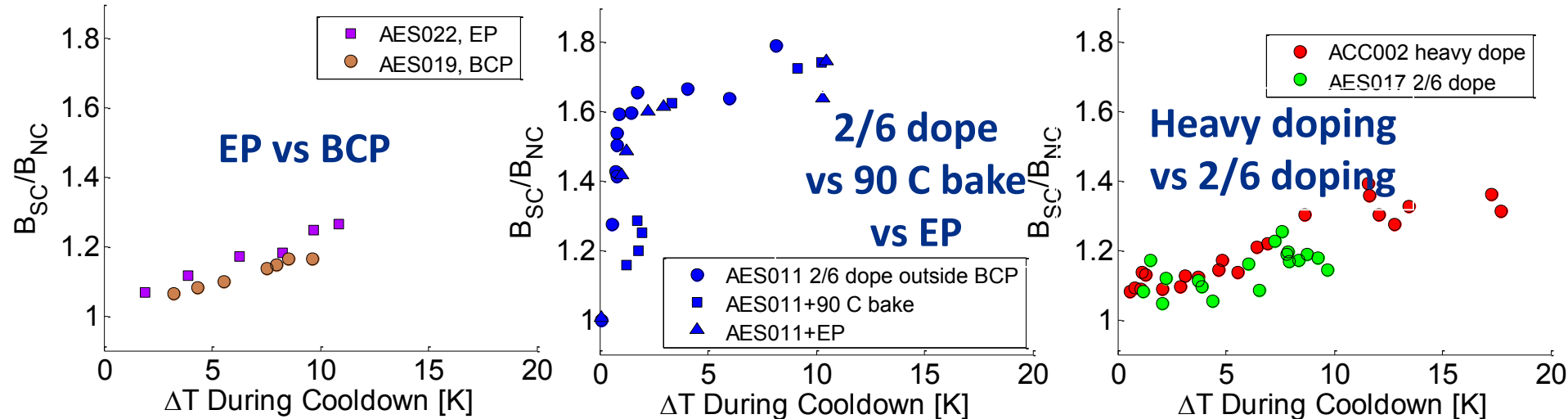
- **Fast cool-down** lead to large thermal gradients which promote efficient flux expulsion
- **Slow cool-down**  $\rightarrow$  poor flux expulsion



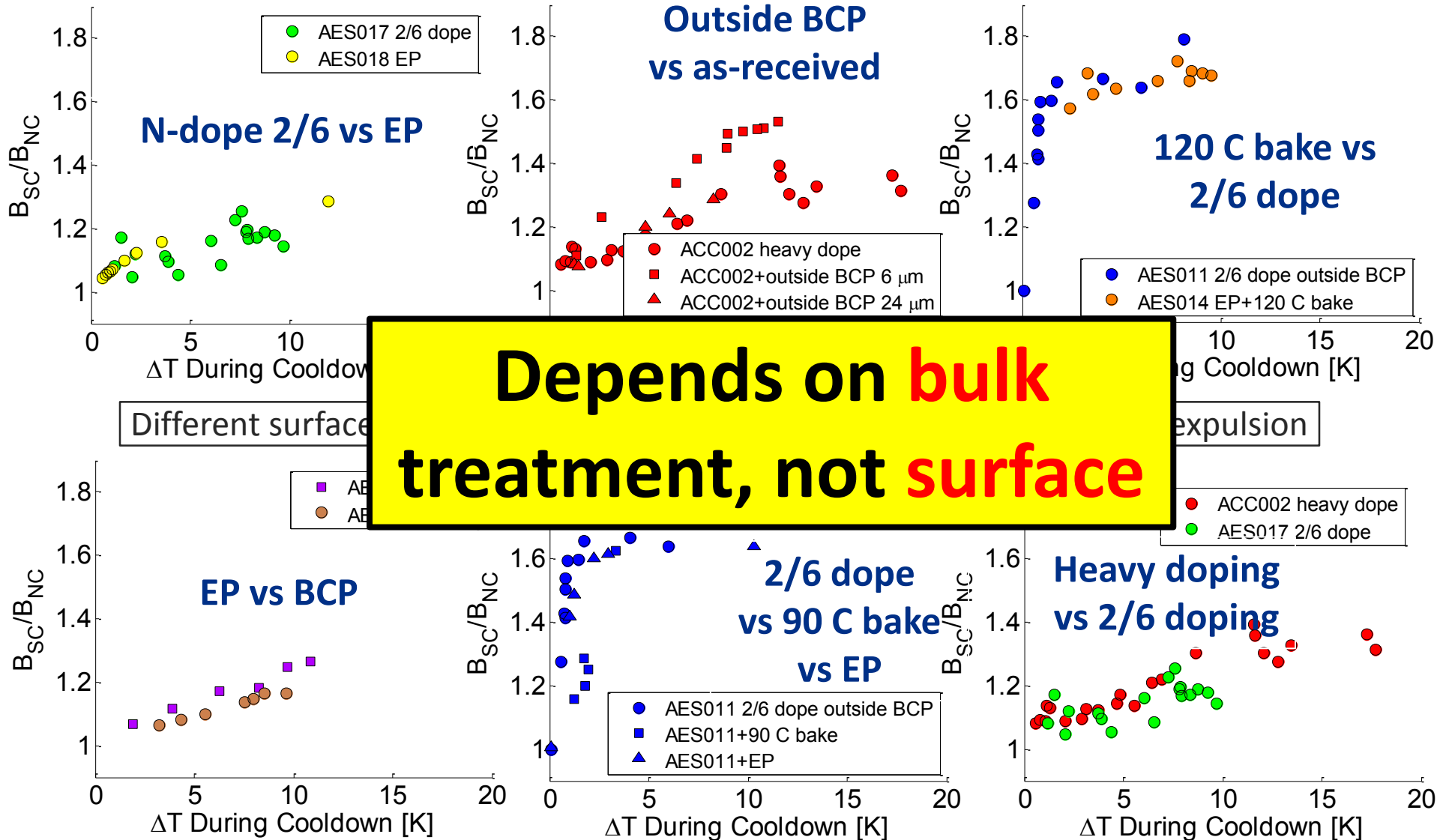
## 2) Surface treatments have insignificant impact



Different surface conditions in cavities with similar bulk history: similar expulsion

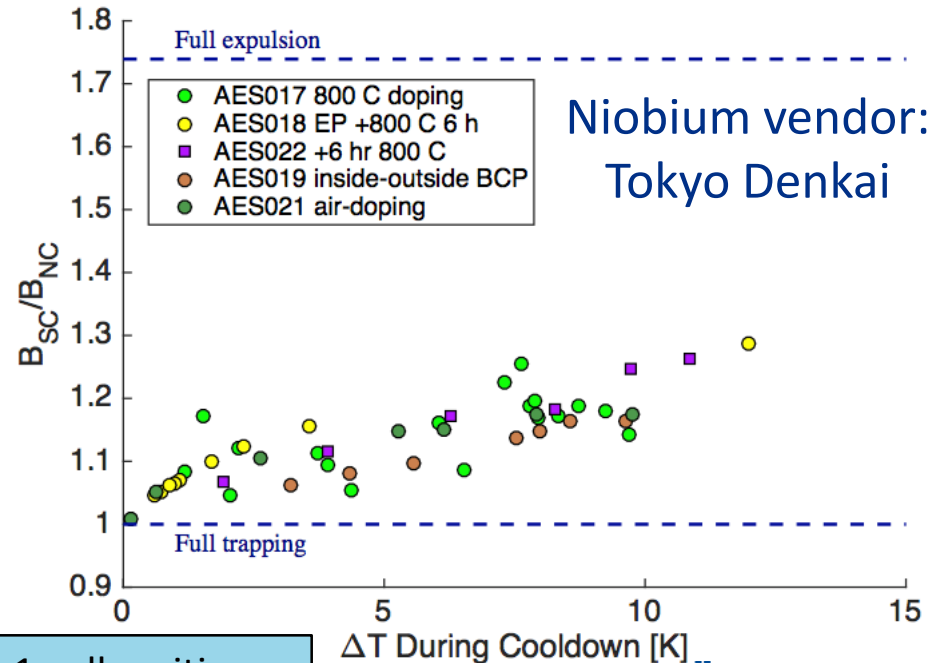
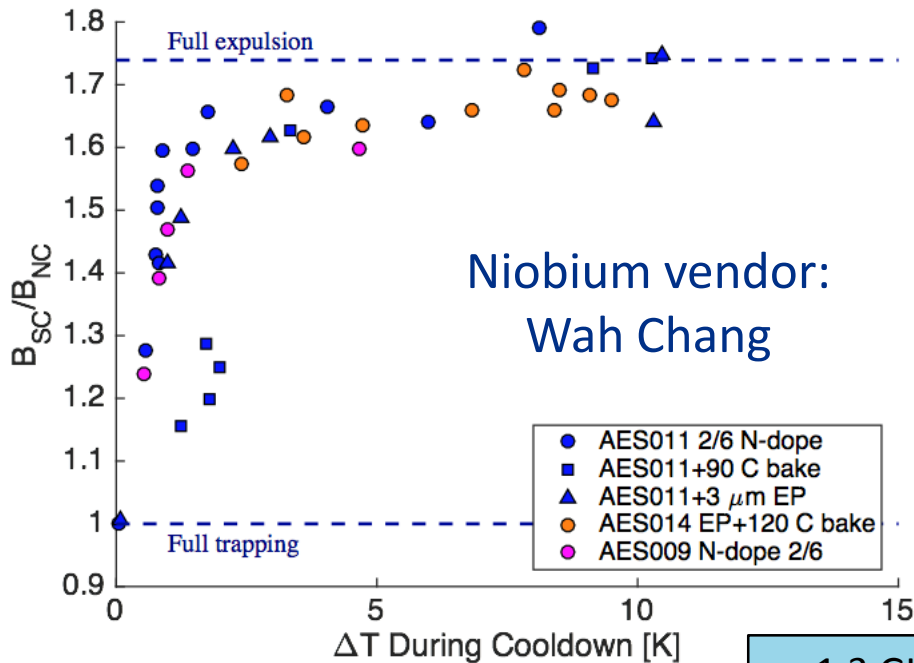


## 2) Surface treatments have insignificant impact



### 3) Some niobium production runs have very poor expulsion – even with large $\Delta T$

- Seems to be a great deal of variability in as-received material
- Variability from batches even within a single vendor



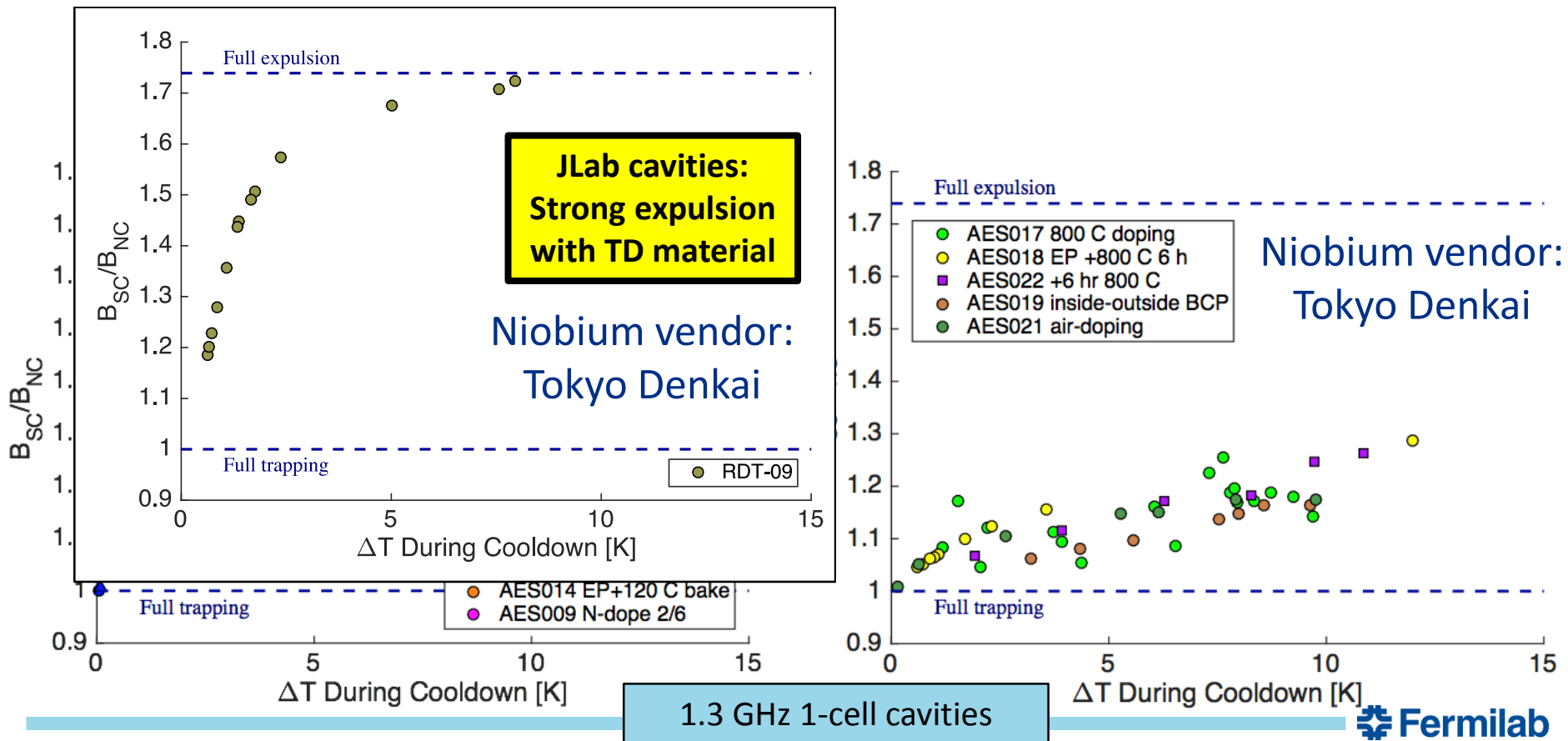
1.3 GHz 1-cell cavities





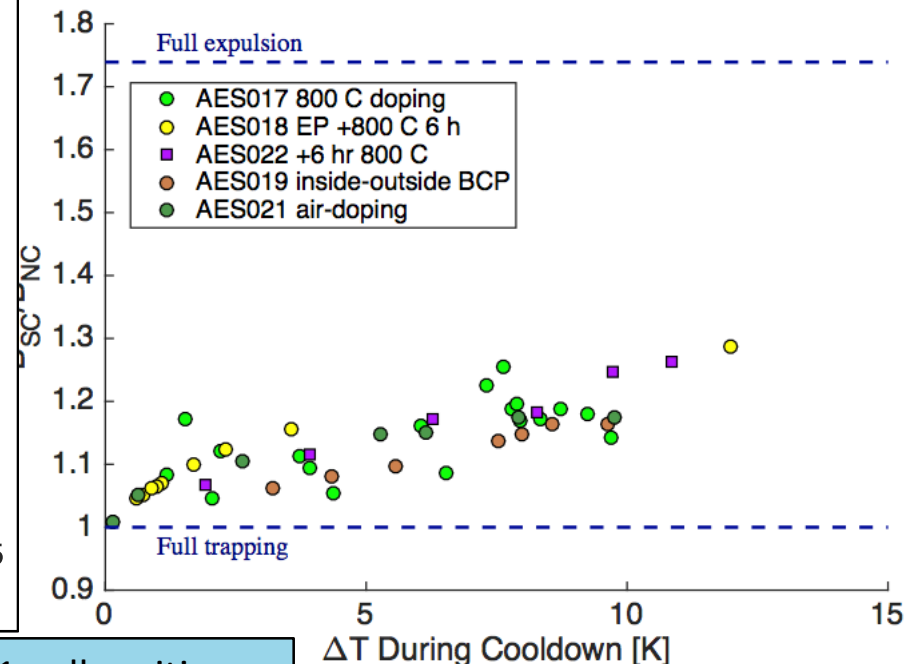
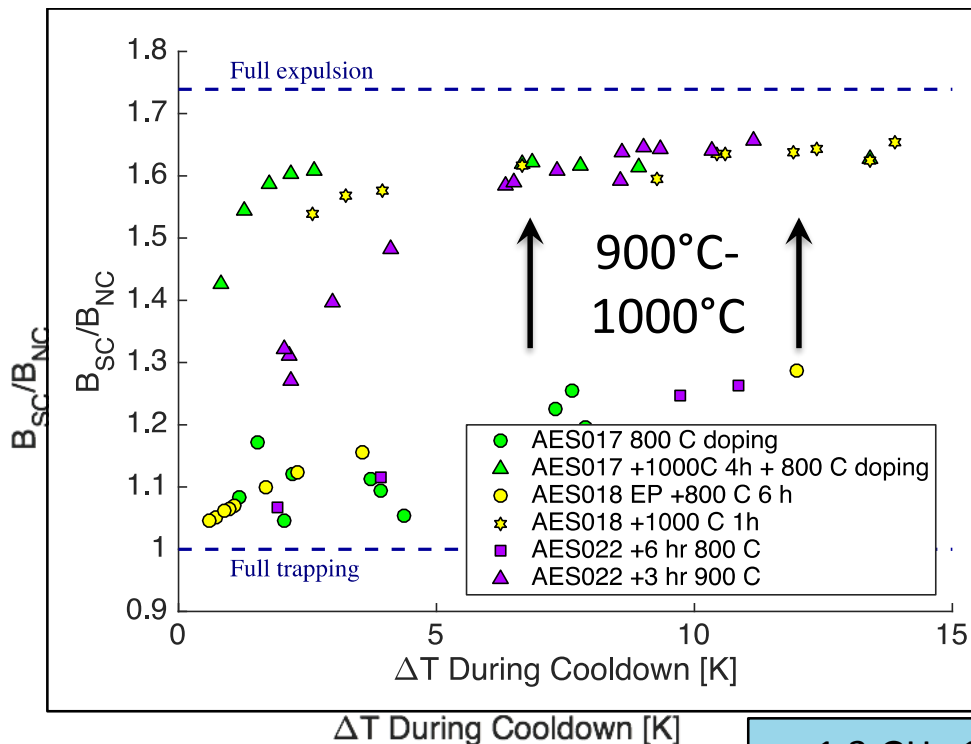
### 3) Some niobium production runs have very poor expulsion – even with large $\Delta T$

- Seems to be a great deal of variability in as-received material
- Variability from batches even within a single vendor



# 4) High temperature treatment can make poorly expelling material expel well even with small $\Delta T$

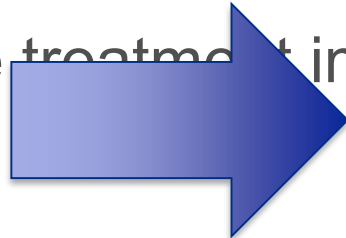
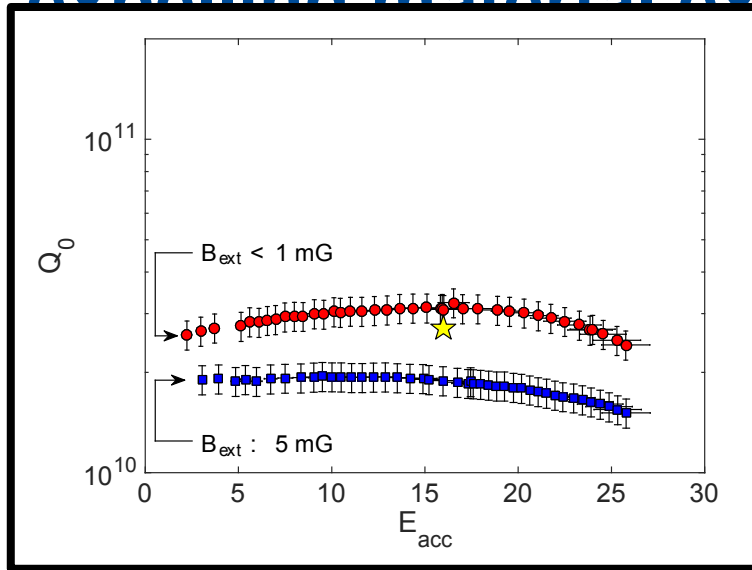
- 900 C – 1000 C furnace treatment improves expulsion



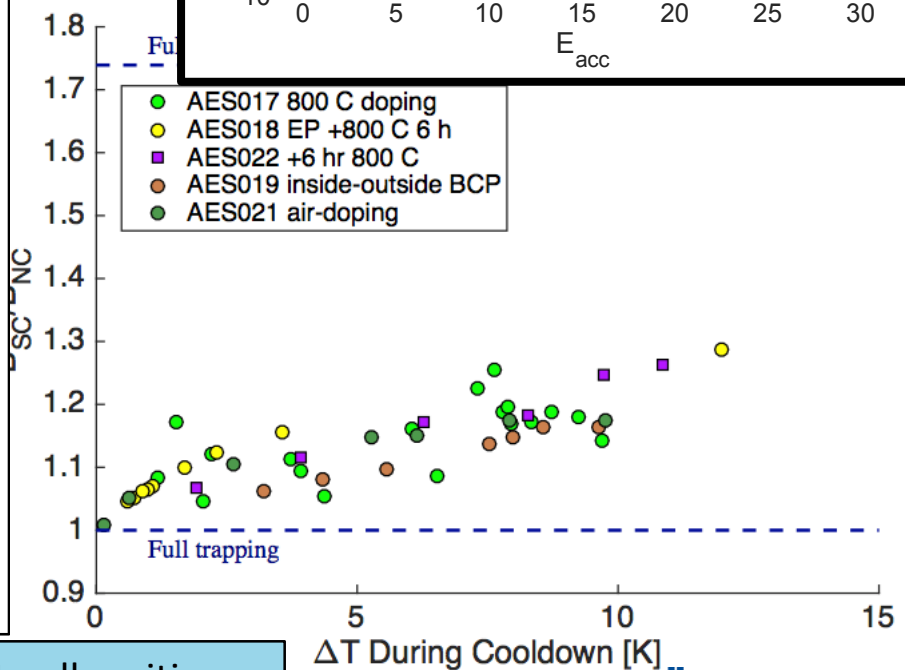
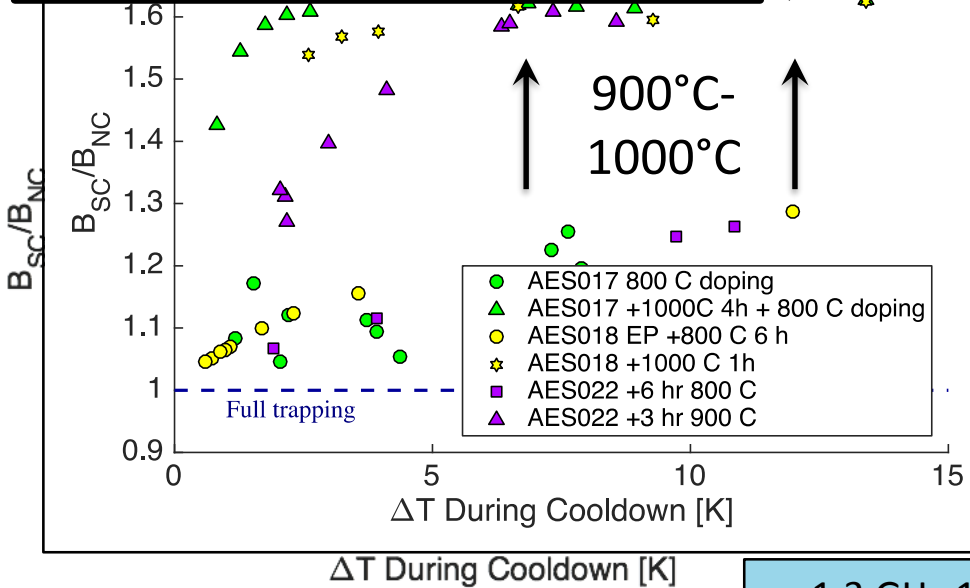
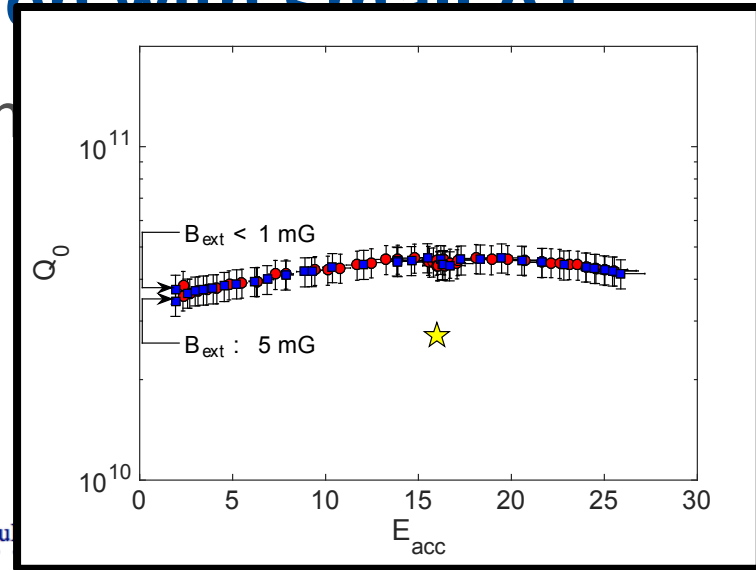
1.3 GHz 1-cell cavities



# 4) High temperature treatment can make poorly expelling material expel well even with small $\Delta T$



900°C treatment

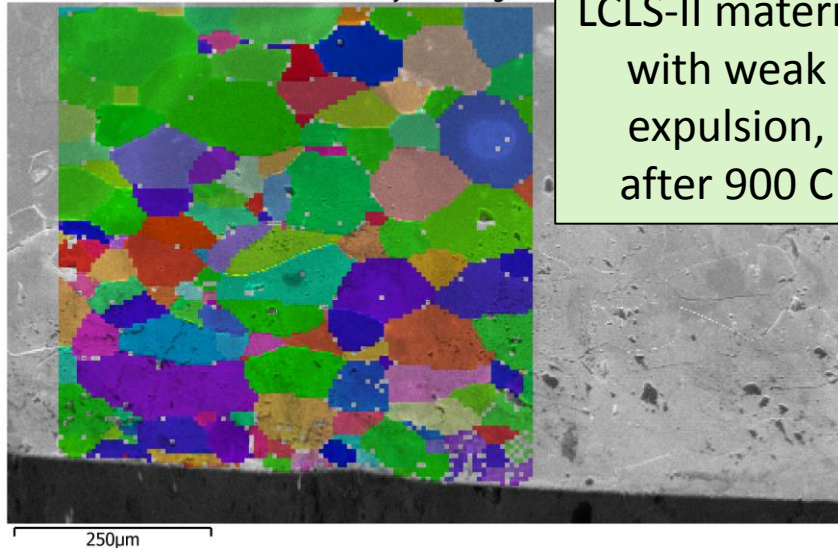


1.3 GHz 1-cell cavities

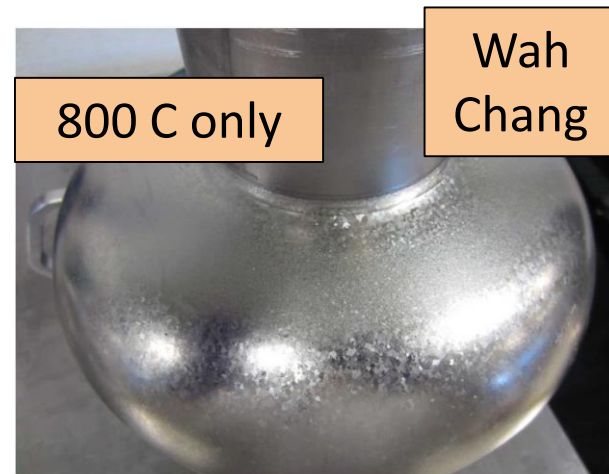
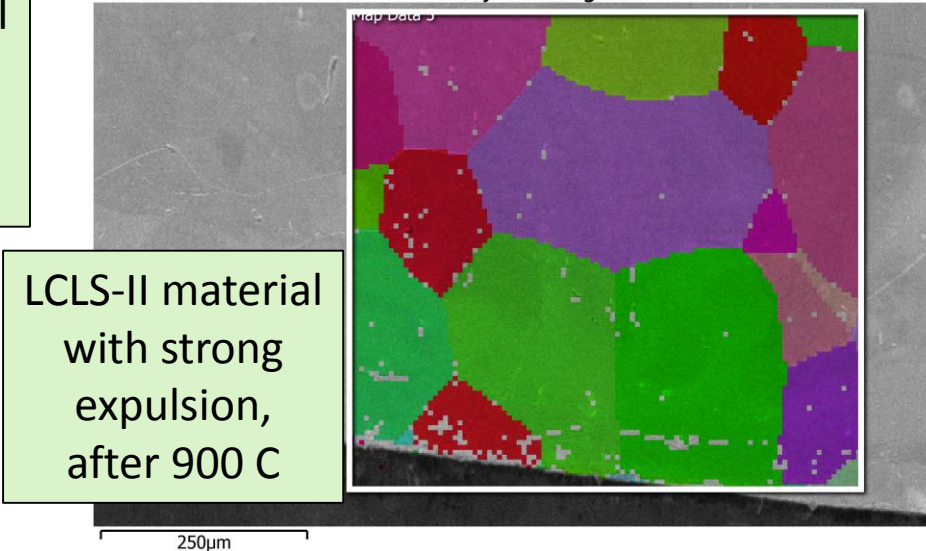


# 5) Improvement in expulsion is correlated with grain growth

EBSD Layered Image 4



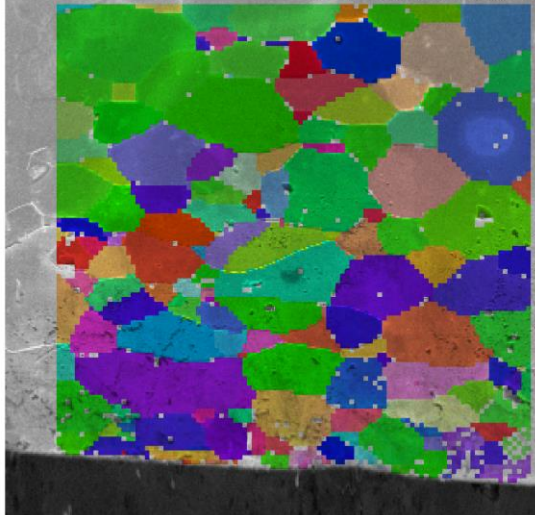
EBSD Layered Image 3





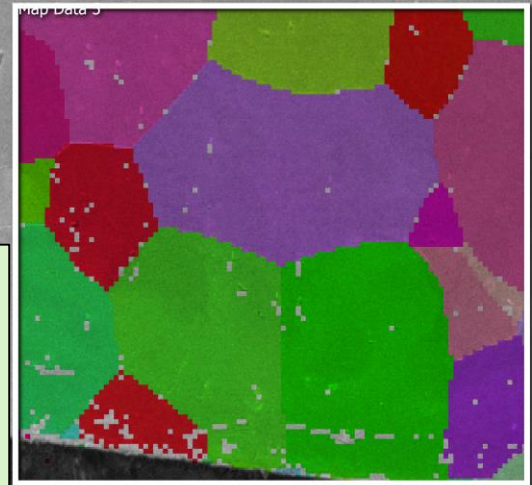
# 5) Improvement in expulsion is correlated with grain growth

EBSD Layered Image 4



LCLS-II material with weak expulsion, after 900 C

EBSD Layered Image 3



LCLS-II material with strong expulsion, after 900 C

**Why is 800 C enough to grow giant grains in some Nb but 1000 C required for others?**

Impurities/RRR? Dislocations?

800 C only

Wah Chang



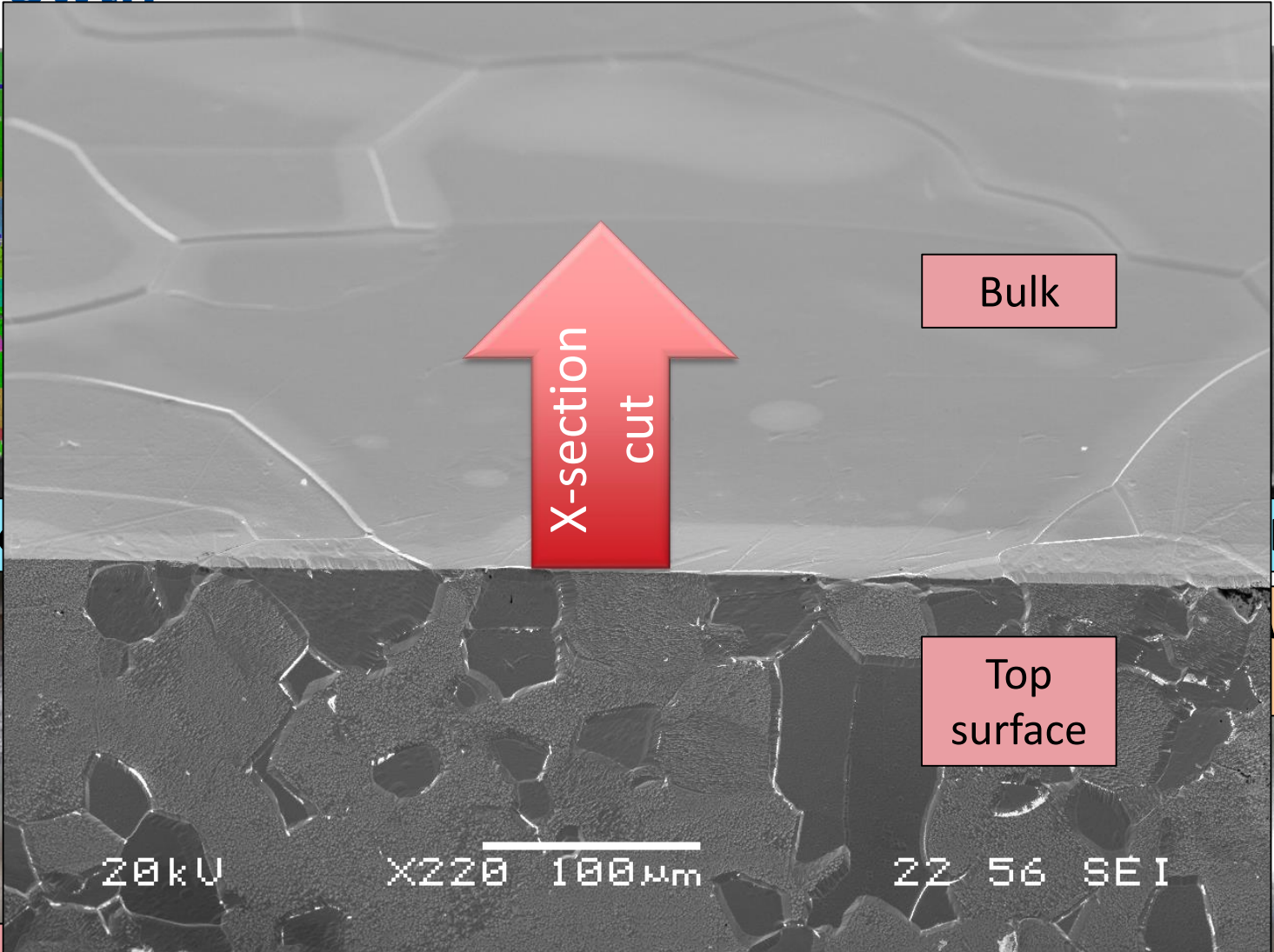
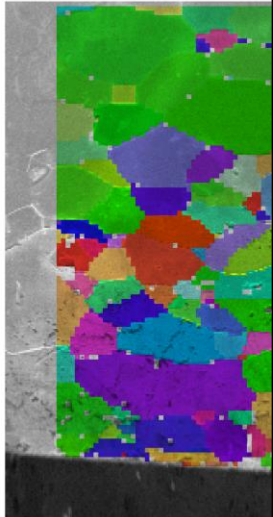
1000 C 4 hrs

Tokyo Denkai





# 5) Improvement in expulsion is correlated with grain growth



Why is 800 C

hers?

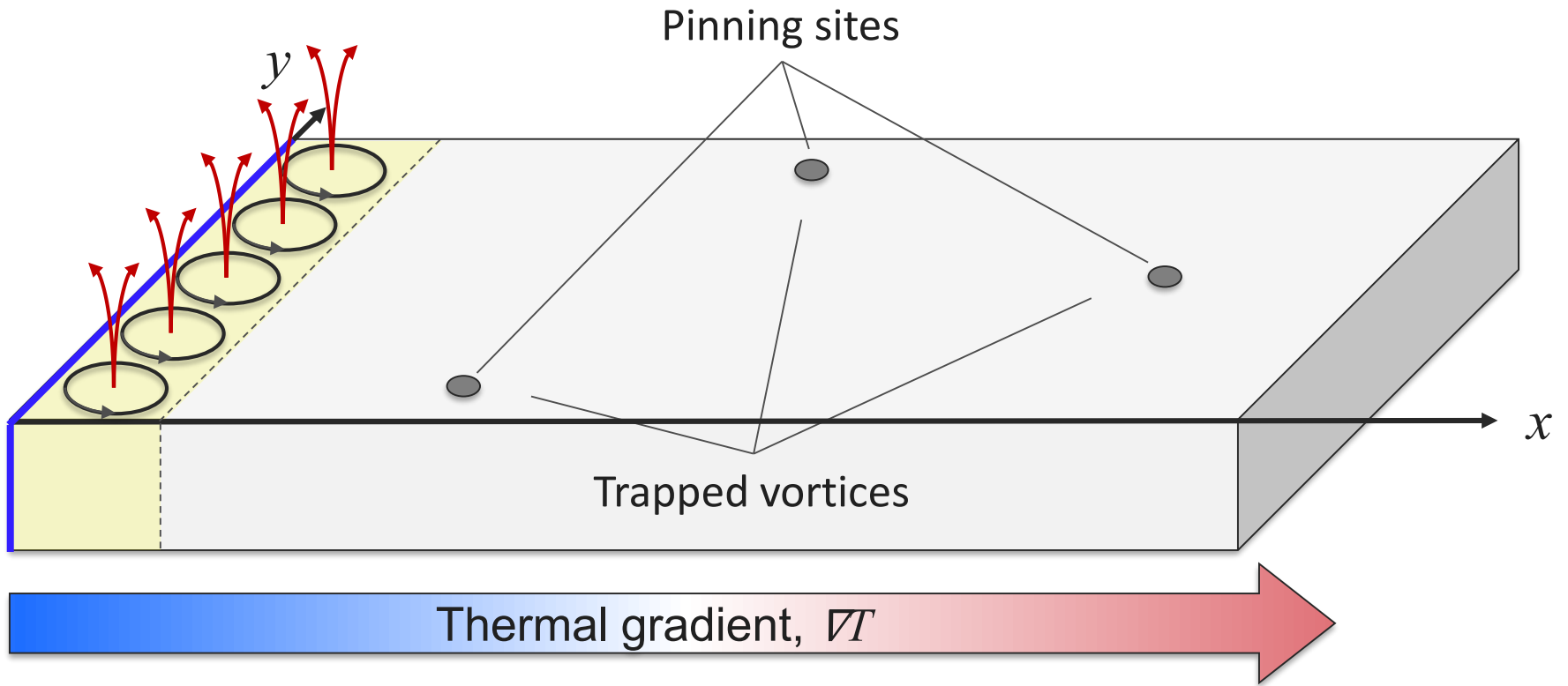
Wah  
hang

1000 C 4 hrs

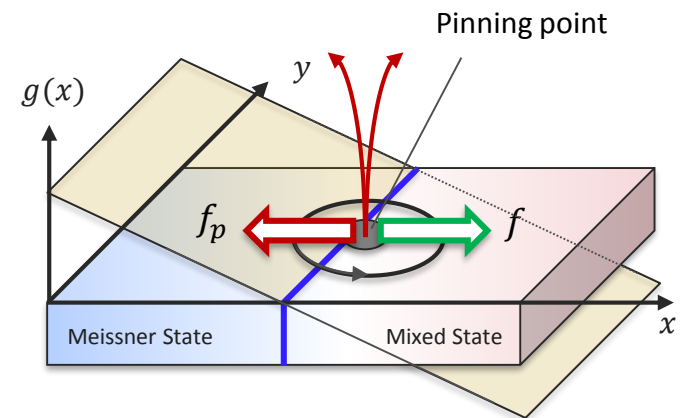
Tokyo  
Denkai



# Model for Flux Expulsion Consistent with 1)-6) Above



- What types of pinning sites are the dominant mechanism for trapping?
- Grain/crystal boundaries? Intragrain dislocations from deformation?



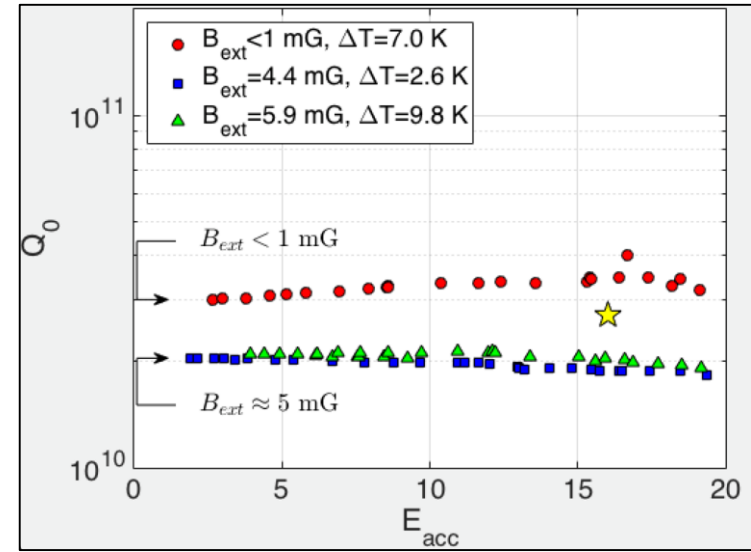
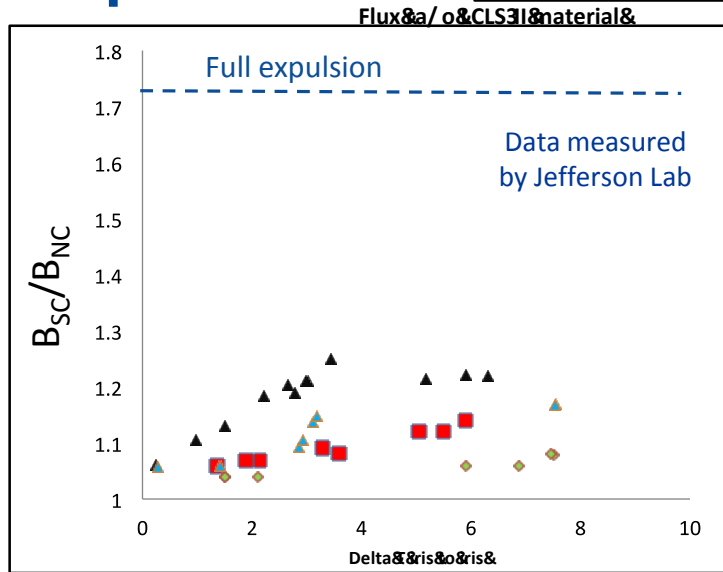
Magnetic Flux Expulsion  
**Material for LCLS-II**

# LCLS-II - Preproduction

1.3 GHz 1-cell  
cavities

Cooling in 5 mG applied field  
(spec for background field in module)

As-received  
niobium  
material for  
LCLS-II  
production:  
very poor  
expulsion





# LCLS-II - Preproduction

1.3 GHz 1-cell  
cavities

Cooling in 5 mG applied field  
(spec for background field in module)

Flux @ 1.3 GHz 1-cell cavities  
Full expansion  
1.8  
1.7

•  $B_{\text{ext}} < 1 \text{ mG}$ ,  $\Delta T = 7.0 \text{ K}$   
■  $B_{\text{ext}} = 4.4 \text{ mG}$ ,  $\Delta T = 2.6 \text{ K}$



U.S. DEPARTMENT OF  
**ENERGY**

## 2.7 Cryomodules

D. Stout, MSU / Subcommittee 7

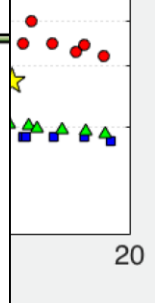
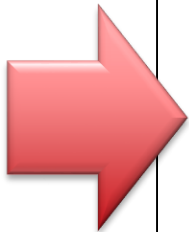
OFFICE OF  
**SCIENCE**

### Recommendations

1. The Project is ready to proceed to CD-2/3
2. Finalize cavity and cryomodule minimum acceptance criteria based on the current project baseline – by 3/2016
3. Conduct a supply chain risk assessment of critical cryomodule assembly components to identify items needing second sources or other mitigations – by 3/2016
4. Develop a cure to improve the flux expulsion of the procured niobium material and implement before cavity production.
5. Conduct an independent peer review of the detailed assembly methods for connecting cryomodules – prior to first connection in 2017

LCLS-II CD2/3 Review Closeout, Dec 2015

As-rec  
niob  
mater  
LCL  
produ  
very  
expu

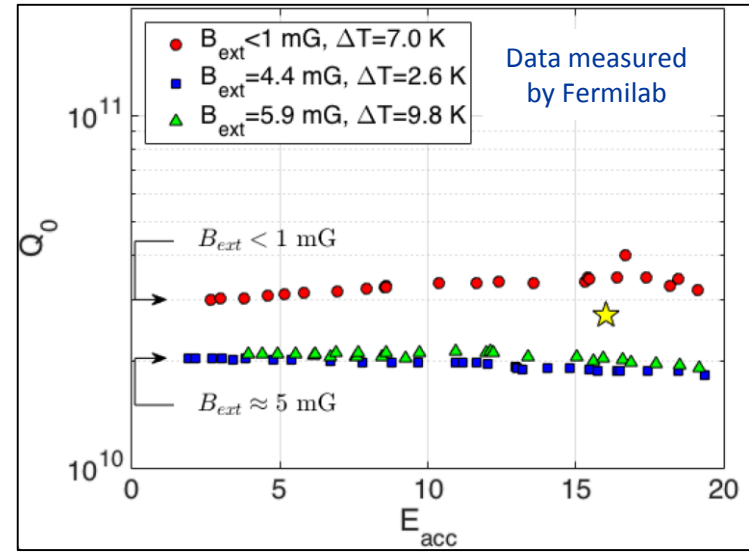
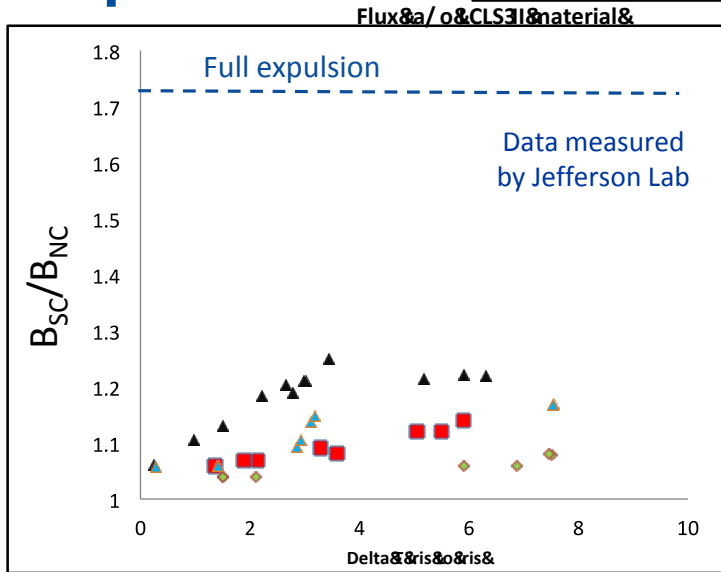


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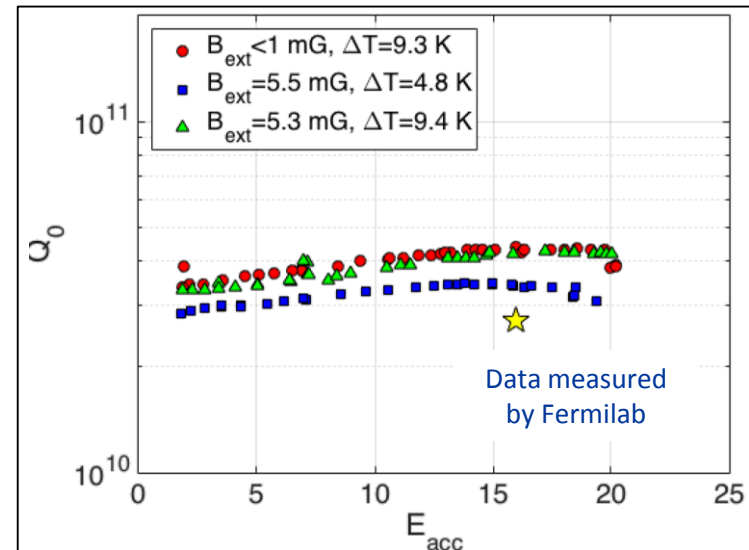
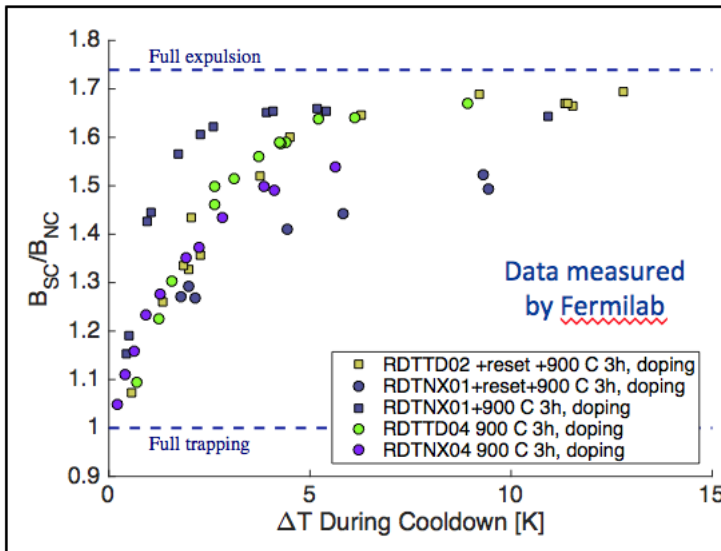
1.3 GHz 1-cell cavities

Cooling in 5 mG applied field  
(spec for background field in module)

As-received niobium material for LCLS-II production: very poor expulsion



After 900°C treatment: much improved



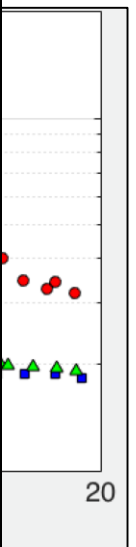
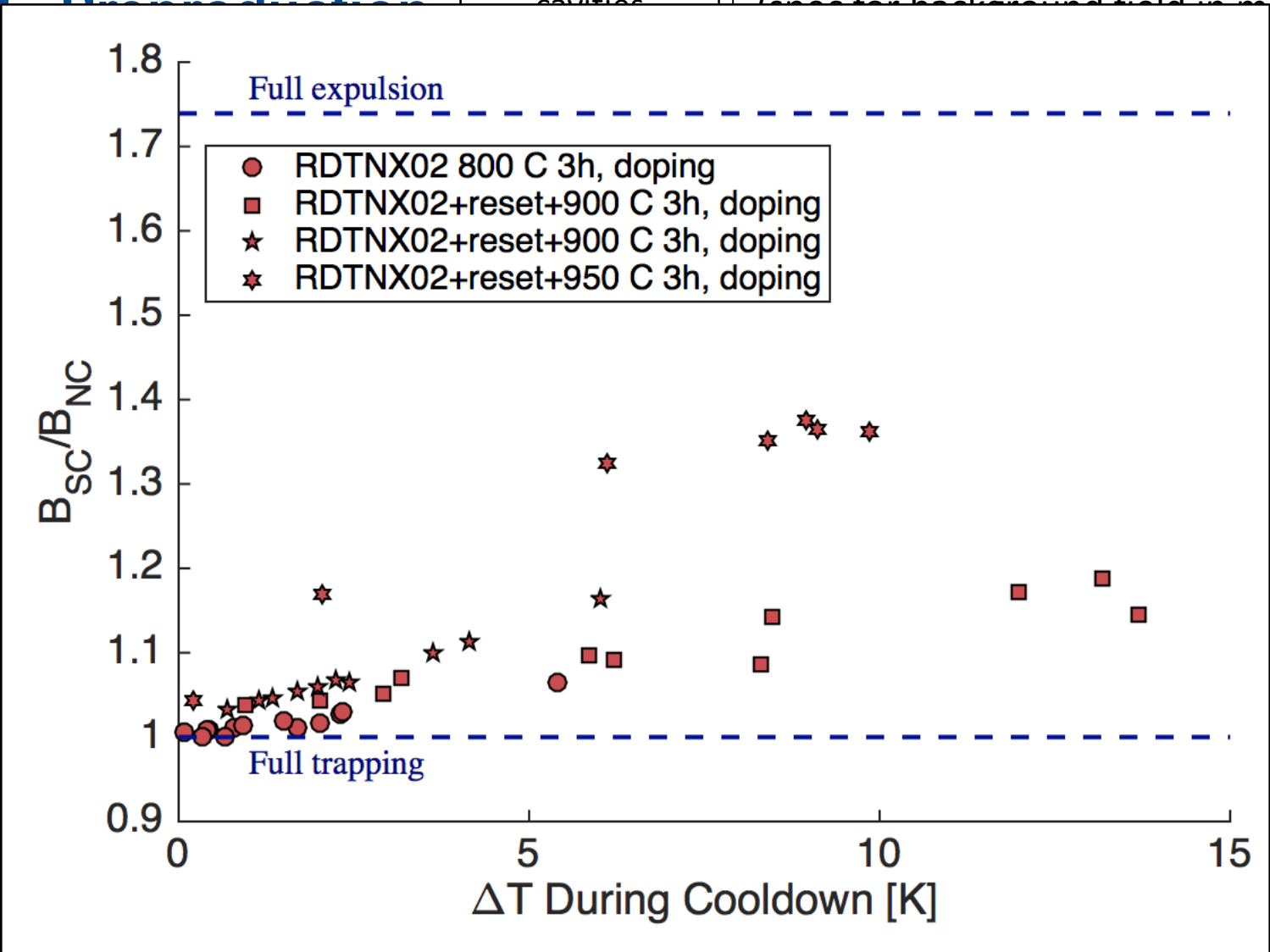
# LCLS-II Production

1.3 GHz 1-cell  
cavities

Cooling in 5 mG applied field  
(less for background field in module)

As-received niobium material for LCLS-II production very poor expulsion

After 900° treatment much improved

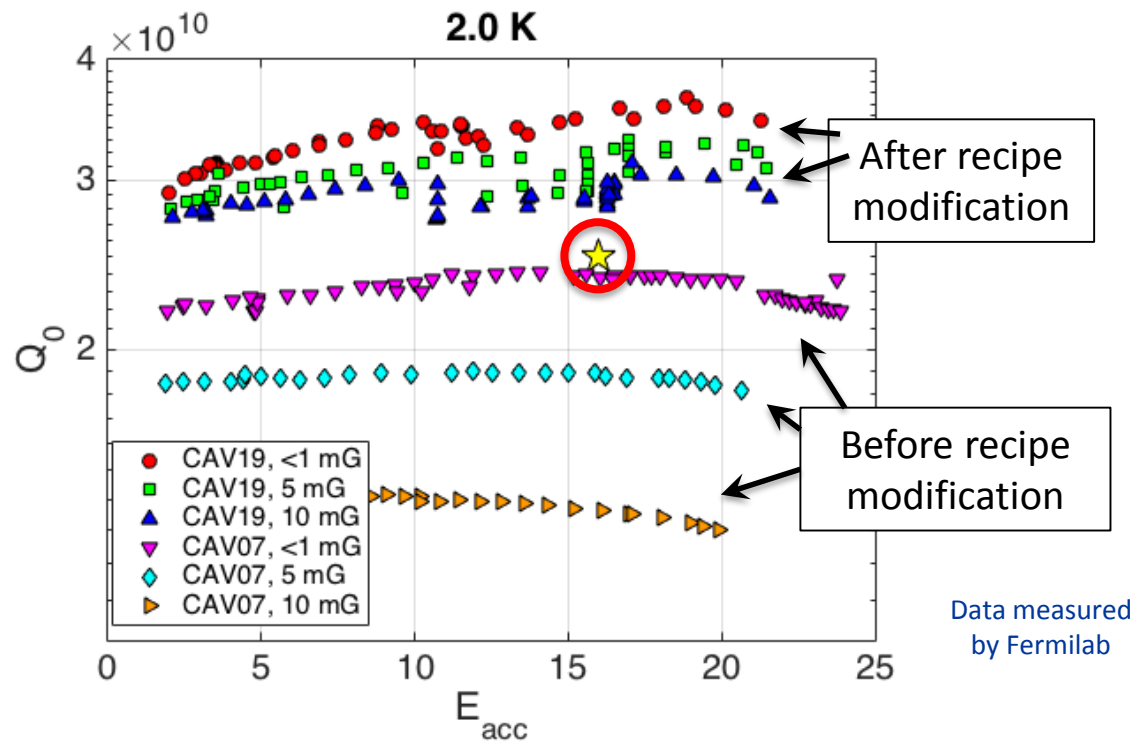


“Lot C” material – lower RRR, smaller grains (details in talk from Ari Palczewski)



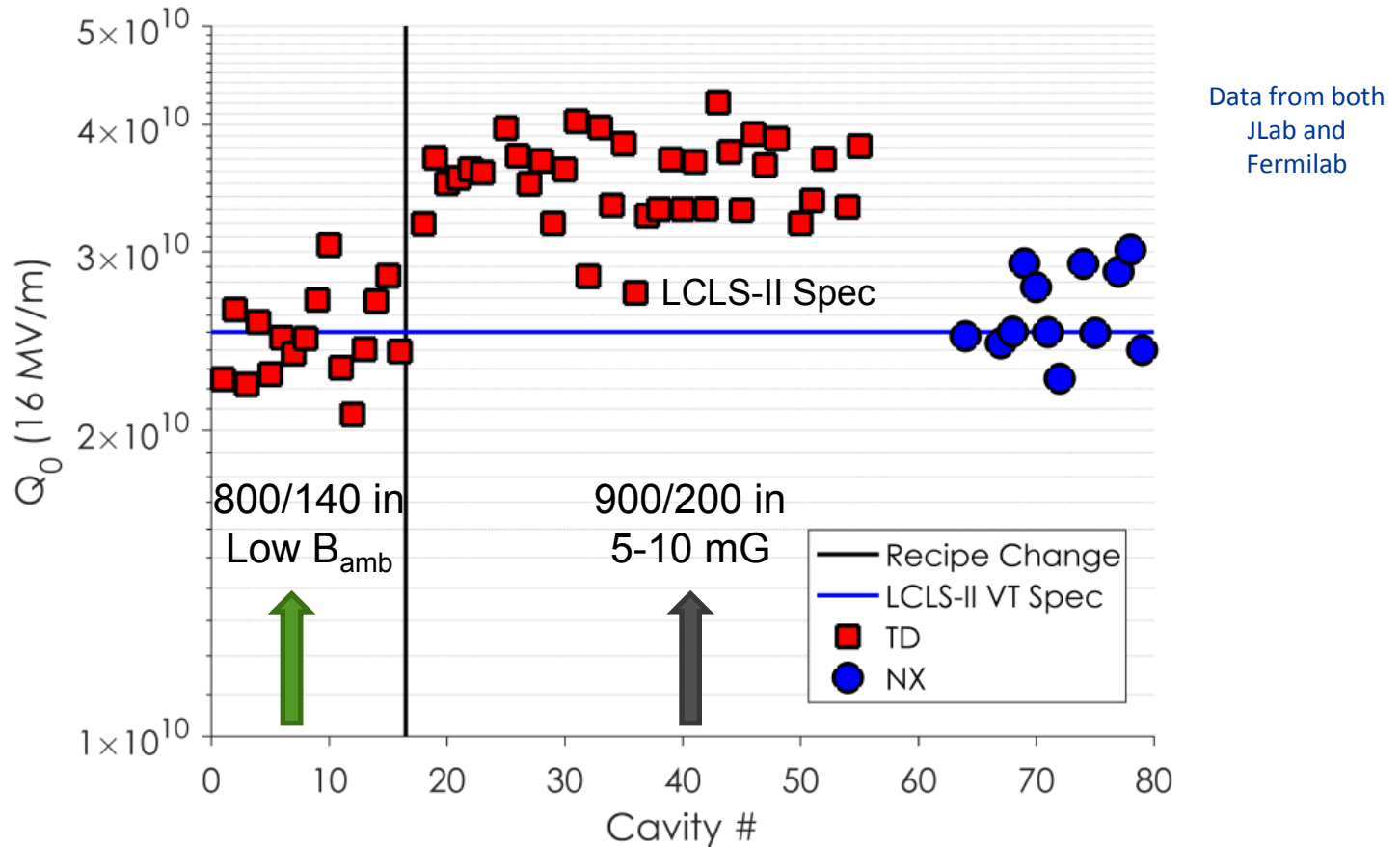
# LCLS-II - Production

- See below difference between flux trapping in baseline 800 C recipe compared to 900 C modification
- These are production 9-cell cavities that are now in cryomodules for LCLS-II



# LCLS-II Production Cavity $Q_0$ Before/After Recipe Change

## Cavity $Q_0$ Performance in VT





# Why Flux Expulsion is Important

Cavity	Usable Gradient* [MV/m]	Q0 @ 16 MV/m (or useable gradient) 2 K
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<b>Total Voltage</b>	<b>166 MV</b>	

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CAV0029	21.0	4.4E+10
CAV0042	16.8	2.8E+10
CAV0032	21.0	3.0E+10
<b>Average</b>	<b>17.6</b>	<b>3.5E+10</b>
<b>Total Voltage</b>	<b>146.4</b>	

Fermilab CM-2  
**Baseline recipe: 800 C  
 degas, 140 μm bulk EP  
 Fast cooldown**

Fermilab CM-3  
**Modified recipe: 900 C  
 degas, 200 μm bulk EP  
 Fast cooldown**

Total voltage Spec: 133 MV

Q<sub>0</sub> Spec: 2.7x10<sup>10</sup>

Magnetic Flux Expulsion  
**Additional Experiments**

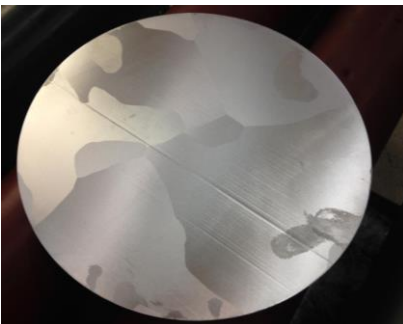
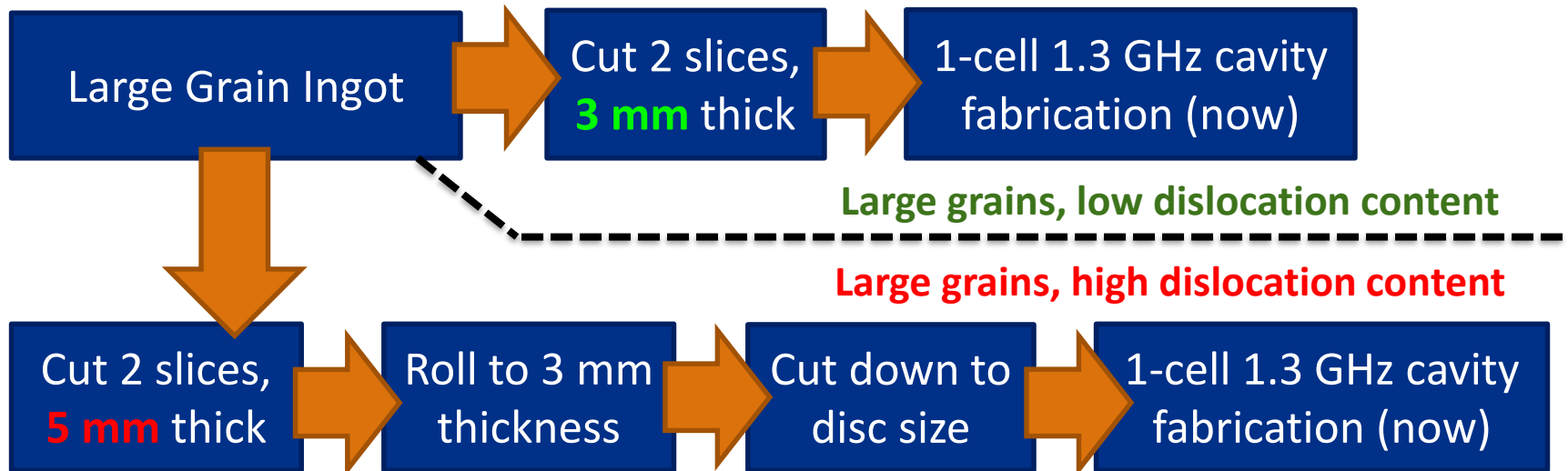
## Future High $Q_0$ Cavity Production

- The activity to ‘cure’ the flux expulsion in LCLS-II cavities put a strain on the project
- For future procurement of niobium for high  $Q_0$  cavity production, it is **crucial to understand how to improve specifications**
- In parallel: experiments to further develop understanding of physical mechanisms that control trapping/expulsion during cooldown



# Large Grain Experiment

Experiment designed to distinguish effects of dislocations independent of grain size: does LG material inherently expel strongly?



# Acknowledgements

- Intellectual and experimental contributions to this experimental endeavor from Sebastian Aderhold, Mattia Checchin, Curtis Crawford, Anna Grassellino, Martina Martinello, Alex Melnychuk, Hasan Padamsee, Roman Pilipenko, Alexandr Romanenko, Dmitri Sergatskov, Yulia Trenikhina
- Special thanks to Fermilab VTS teams
- Special thanks to LCLS-II, Jefferson Lab, SLAC for data and niobium samples relevant to LCLS-II

# Summary

- Flux expulsion experiment handbook:
  1. Large thermal gradients at  $T_c$  promote expulsion of flux
  2. Surface treatments have insignificant impact
  3. Some niobium production runs have very poor expulsion (even with large  $\Delta T$ )
  4. High temperature treatment can make poorly expelling material expel well (even with small  $\Delta T$ )
  5. Improvement in expulsion is correlated with grain growth
  6. Heavy deformation degrades expulsion behavior
- Experiments continue to boost understanding of flux expulsion physics and improve material specifications for future projects