Longitudinal Phase Space Dynamics in ERLs

S. Benson, D. Douglas, C. Tennant,
Jefferson Lab, 12000 Jefferson Avenue, Newport News,
Virginia, 23606 USA

Pavel Evtushenko, Helmoltz Zentrum Dresden Rossendorf.

Dresden, Germany

Presented at the Energy Recovery Workshop 2019
Berlin Germany, 16-20 September 2019



Outline

- General features of longitudinal matches
- FEL match
- NP match
- Cooling match
- Conclusions

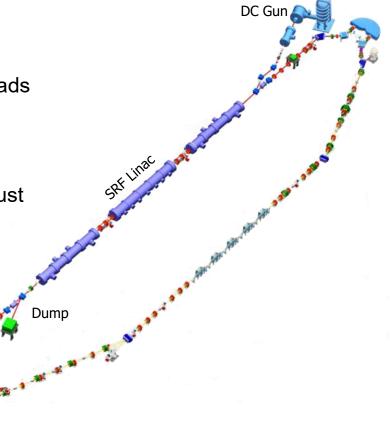
Top-Level Features of ERL Architectures

- Motivation for ERL architecture: save money on RF drive while delivering bright high power beams
 - ideal ERLs have P_{beam} >> P_{RF}; involve very high CW beam powers
 - beam quality preservation and control of paramount importance
- ERLs are basically just time-of-flight spectrometers
 - they exist to create specific conspiracies between time and energy
 - longitudinal motion ("longitudinal match") must be carefully controlled
- ERLs are non-equilibrium systems
 - ERLs look like rings, but behave like injector chains
 - high power beam ⇒ "injection efficiency" (99.999+%) critical
 - beam and lattice are different, and beam is not Gaussian
 - beam and lattice may evolve independently, be mismatched
 - Beam degrades at the target and then gets anti-damped.



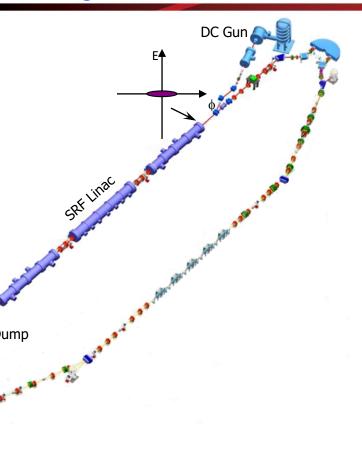
Requirements on phase space:

- high peak current (short bunch) at FEL
 - bunch length compression at wiggler using quads and sextupoles to adjust compactions
- "small" energy spread at dump
 - energy compress while energy recovering
 - "short" RF wavelength/long bunch, large exhaust δp/p (~10%)
 - ⇒get slope, curvature, *and* torsion right (quads, sextupoles, octupoles)
- Note that this is a parallel-to-point longitudinal match



Requirements on phase space:

- high peak current (short bunch) at FEL
 - bunch length compression at wiggler using quads and sextupoles to adjust compactions
- "small" energy spread at dump
 - energy compress while energy recovering
 - "short" RF wavelength/long bunch, large exhaust δp/p (~10%)
 - ⇒get slope, curvature, *and* torsion right (quads, sextupoles, octupoles)
- Note that this is a parallel-to-point longitudinal match









Nonlinear FEL Longitudinal Matching

As shown earlier – but with typical "real" bunch shapes DC Gun RF curvature can degrade compressed bunch length Set nonlinear momentum compaction with sextupoles to compensate & linearize bunch Avoids use of harmonic RF (expensive/constrains aperture) Energy compression during recovery – • "short" RF wavelength/ultimately long bunch (30°+), large exhaust $\delta p/p$ (~10-15%) ⇒get slope, curvature, and torsion right (quads, sextupoles, octupoles...) to match bunch to RF waveform.

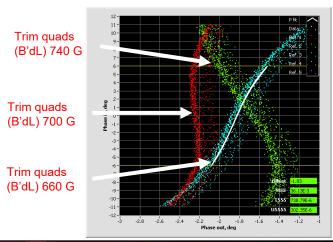


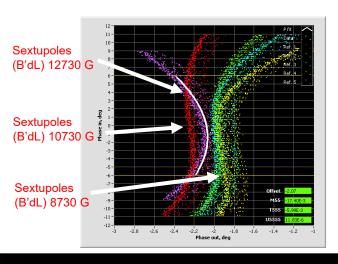
lasing extracts energy and increases energy

spread

JLab FEL bunch compression and diagnostics

- The Jlab FEL operated with a bunch compression ratio of 17–25 using <u>nonlinear compression</u> compensating for LINAC RF curvature (up to 2nd order during acceleration and 3rd order during recovery).
- The RF curvature compensation is made <u>with multipoles</u> installed in dispersive locations of 180° Bates bend with separate function magnets <u>no harmonic RF</u>
- Operationally longitudinal match relies on:
 - a. Longitudinal transfer function measurements R₅₅, T₅₅₅, U₅₅₅₅
 - b. Bunch length measurements at full compression (Martin-Puplett Interferometer)
 - c. Energy spread measurements in injector and exit of the LINAC





- R₅₆ and T₅₆₆ are validated via longitudinal transfer function measurements.
- Arrival phase is measured with a pillbox cavity + heterodyne receiver.
- Phase of the injector is modulated relative to the LINAC phase
- Essential ~ 15 % energy acceptance and ~ 30 % phase acceptance

Connecting R₅₆ & T₅₆₆ to M₅₅

$$\varphi_{W} = \left(1 + R_{56}^{C} \cdot R_{65}^{L}\right) \varphi_{0} + \left[R_{56}^{C} \cdot T_{655}^{L} + \left(R_{65}^{L}\right)^{2} \cdot T_{566}^{C}\right] \varphi_{0}^{2} \quad \text{taking second order transport matrix elements}$$

- R₅₆ and T₅₆₆ are validated via longitudinal transfer function measurements.
- Arrival phase is measured with a pillbox cavity + heterodyne receiver.
- Phase of the injector is modulated relative to the LINAC phase
- Essential ~ 15 % energy acceptance and ~ 30 % phase acceptance

$$\begin{split} \varphi_W = & \left(1 + R_{56}^C \cdot R_{65}^L \right) \varphi_0 + \left[R_{56}^C \cdot T_{655}^L + \left(R_{65}^L \right)^2 \cdot T_{566}^C \right] \varphi_0^2 \quad \text{taking second order transport matrix elements} \\ & R_{55}^{inj \to w} = 1 + R_{56}^C \cdot R_{65}^L \\ & T_{555}^{inj \to w} = R_{56}^C \cdot T_{655}^L + \left(R_{65}^L \right)^2 \cdot T_{566}^C \end{split}$$

- R₅₆ and T₅₆₆ are validated via longitudinal transfer function measurements.
- Arrival phase is measured with a pillbox cavity + heterodyne receiver.
- Phase of the injector is modulated relative to the LINAC phase
- Essential ~ 15 % energy acceptance and ~ 30 % phase acceptance

$$\varphi_W = \left(1 + R_{56}^C \cdot R_{65}^L\right) \varphi_0 + \left[R_{56}^C \cdot T_{655}^L + \left(R_{65}^L\right)^2 \cdot T_{566}^C\right] \varphi_0^2 \quad \text{taking second order transport matrix elements}$$

$$R_{55}^{inj \to w} = 1 + R_{56}^C \cdot R_{65}^L$$

$$T_{555}^{inj \to w} = R_{56}^C \cdot T_{655}^L + \left(R_{65}^L\right)^2 \cdot T_{566}^C$$
 are adjusted in compressor

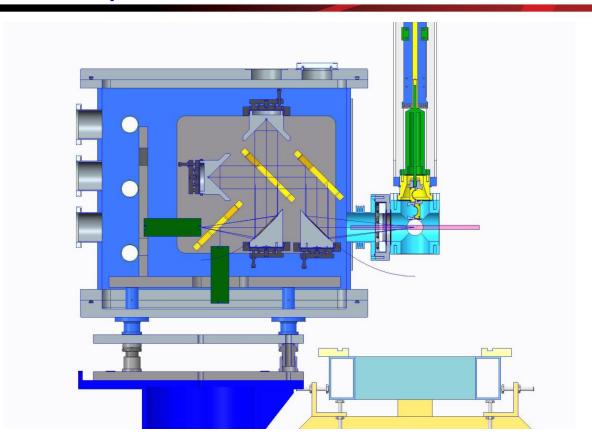
- R₅₆ and T₅₆₆ are validated via longitudinal transfer function measurements.
- Arrival phase is measured with a pillbox cavity + heterodyne receiver.
- Phase of the injector is modulated relative to the LINAC phase
- Essential ~ 15 % energy acceptance and ~ 30 % phase acceptance

$$\varphi_W = \left(1 + R_{56}^C \cdot R_{65}^L\right) \varphi_0 + \left[R_{56}^C \cdot T_{655}^L + \left(R_{65}^L\right)^2 \cdot T_{566}^C\right] \varphi_0^2 \quad \text{taking second order transport matrix elements}$$
 directly
$$R_{55}^{inj \to w} = 1 + R_{56}^C \cdot R_{65}^L$$
 measured
$$T_{555}^{inj \to w} = R_{56}^C \cdot T_{655}^L + \left(R_{65}^L\right)^2 \cdot T_{566}^C$$
 are adjusted in compressor

- R₅₆ and T₅₆₆ are validated via longitudinal transfer function measurements.
- Arrival phase is measured with a pillbox cavity + heterodyne receiver.
- Phase of the injector is modulated relative to the LINAC phase
- Essential ~ 15 % energy acceptance and ~ 30 % phase acceptance

ELBE – Martin-Puplett Interferometer

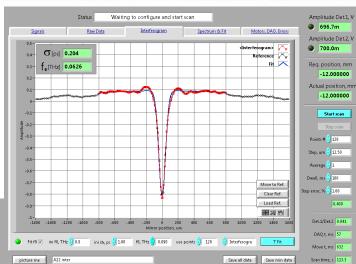
- Interferometer for ELBE proper Martin-Puplett interferometer
- Wire-grid polarizers scaled down by factor 2 to allow shorter than 50 fs measurements
- Built with vacuum chamber to reduce air absorption

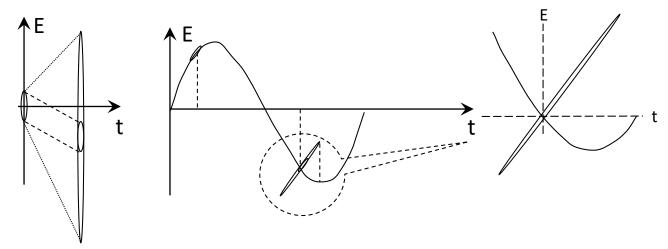


MPI @U37 - Data Evaluation

- At IR/UV Upgrade interferometer data evaluation bunch length extraction was made in frequency domain, NLSF + Gaussian beam assumption
- With ELBE MPI data frequency domain fit is often difficult
- Changed to data evaluation with time domain NLSF
- Always used all data points for fit
- Much more robust

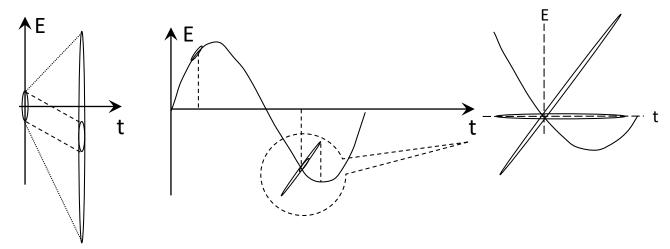






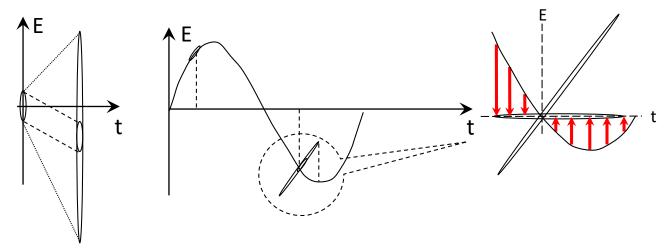
- Beam central energy drops, relative beam energy spread grows
- Recirculator and beam central energies must match to maximize acceptance
- Beam rotated, curved, torqued to match shape of RF waveform
- Maximum energy can't exceed peak deceleration available from linac
 - Corollary: entire bunch must precede trough of RF waveform





- Beam central energy drops, relative beam energy spread grows
- Recirculator and beam central energies must match to maximize acceptance
- Beam rotated, curved, torqued to match shape of RF waveform
- Maximum energy can't exceed peak deceleration available from linac
 - Corollary: entire bunch must precede trough of RF waveform



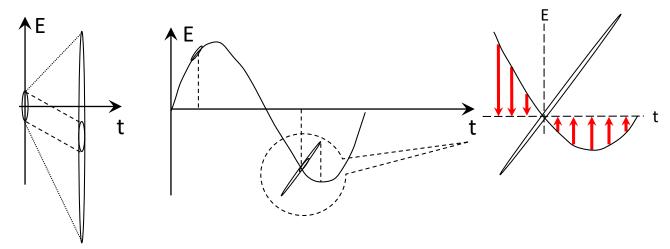


- Beam central energy drops, relative beam energy spread grows
- Recirculator and beam central energies must match to maximize acceptance

10

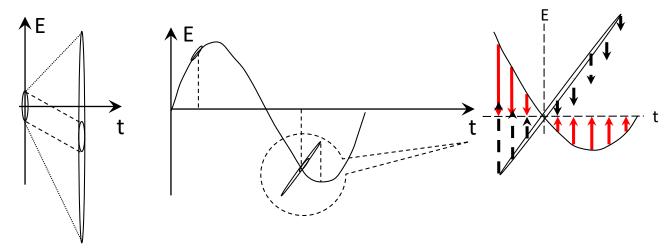
- Beam rotated, curved, torqued to match shape of RF waveform
- Maximum energy can't exceed peak deceleration available from linac
 - Corollary: entire bunch must precede trough of RF waveform





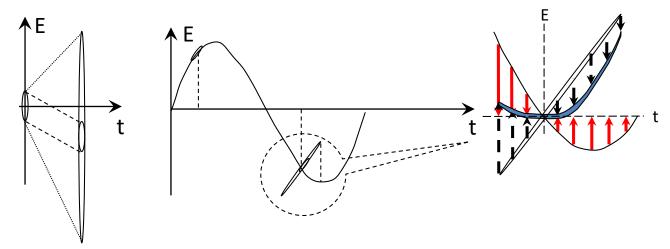
- Beam central energy drops, relative beam energy spread grows
- Recirculator and beam central energies must match to maximize acceptance
- Beam rotated, curved, torqued to match shape of RF waveform
- Maximum energy can't exceed peak deceleration available from linac
 - Corollary: entire bunch must precede trough of RF waveform





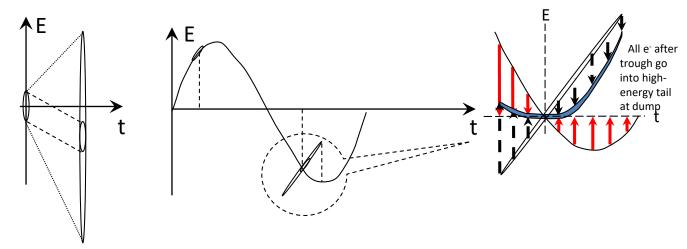
- Beam central energy drops, relative beam energy spread grows
- Recirculator and beam central energies must match to maximize acceptance
- Beam rotated, curved, torqued to match shape of RF waveform
- Maximum energy can't exceed peak deceleration available from linac
 - Corollary: entire bunch must precede trough of RF waveform





- Beam central energy drops, relative beam energy spread grows
- Recirculator and beam central energies must match to maximize acceptance
- Beam rotated, curved, torqued to match shape of RF waveform
- Maximum energy can't exceed peak deceleration available from linac
 - Corollary: entire bunch must precede trough of RF waveform





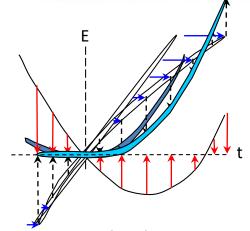
- Beam central energy drops, relative beam energy spread grows
- Recirculator and beam central energies must match to maximize acceptance
- Beam rotated, curved, torqued to match shape of RF waveform
- Maximum energy can't exceed peak deceleration available from linac
 - Corollary: entire bunch must precede trough of RF waveform



10

Higher Order Corrections

- Without nonlinear corrections, phase space becomes distorted during deceleration
- Curvature, torsion,... can be compensated by nonlinear adjustments
 - differentially move phase space regions to match gradient required for energy compression
- Required phase bite is cos⁻¹(1-∆E_{FEL}/E_{LINAC}); at modest energy this is
 - >25° at RF fundamental for 10%
 - >30° for 15%
 - typically need 3rd order corrections (octupoles)
 - also need a few extra degrees for tails, phase errors & drifts, irreproducible
 & varying path lengths, etc, so that system operates reliably
- In this context, harmonic RF very hard to use...



$$M_{56} = -\frac{\lambda_{RF}}{2\pi} \left(\frac{E_0}{E_{linac}} \right) \frac{1}{\sin \phi_0}$$

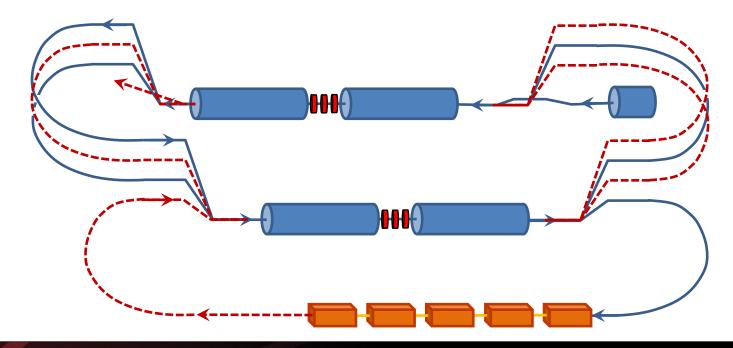
$$T_{566} = -\frac{1}{2} \left(\frac{2\pi}{\lambda_{RF}} \right) (M_{56})^2 \frac{\cos \phi_0}{\sin \phi_0}$$

$$W_{5666} = -\left[\frac{1}{6} + \frac{1}{2} \frac{\cos^2 \phi_0}{\sin^2 \phi_0}\right] \left(\frac{2\pi}{\lambda_{RF}}\right)^2 (M_{56})^3$$

$$U_{56666} \propto \left(\frac{2\pi}{\lambda_{RF}}\right)^3 (M_{56})^4$$
, etc.

Machine Topology for Multipass Machine

- At high energy, a telescopic match is better suited to the requirement for small energy spread but high peak current.
- User separated function arcs to accelerate in two pass up and two passes down.





Longitudinal Matching Solution: Delivery to FEL

- Inject long, low momentum spread bunch
- Initially accelerate on rising portion of RF waveform
- Perform mild compression, full RF curvature compensation at mid-energy
 - **NOTE**: intermediate stages of compression **must** be performed mid-way through acceleration cycle when using multistage compression in an ERL (if transport is common to both accelerated and recovered beams)

13

- Accelerate to full energy on falling portion of RF waveform to de-chirp beam to produce small final momentum spread
- Compress bunch length during transport to FEL

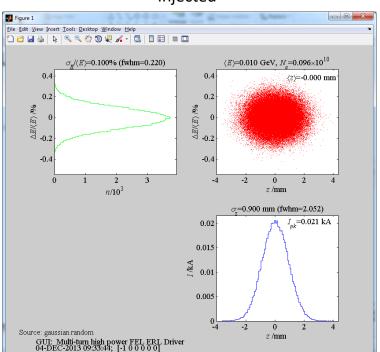


Longitudinal Matching Solution: Energy Recovery

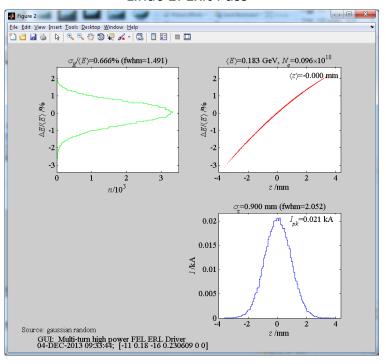
- Complete energy recovery while lasing
 - E_{dump} < E_{injection}
- Multistage nonlinear energy compression during energy recovery
 - Curvature/torsion compensation
 - provides small $\delta p/p$ at dump
 - Keeps E_{dump} constant as FEL turns off/on
 - Defines RF drive requirements (which are modest)



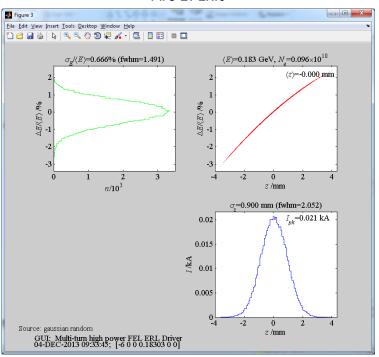




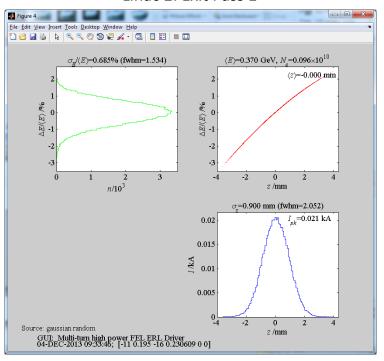
Linac 1: Exit Pass



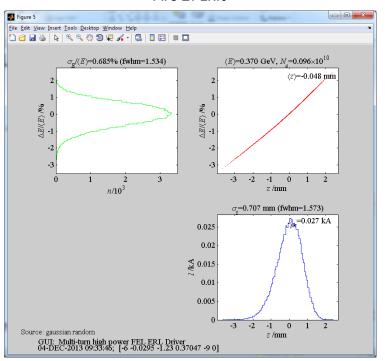
Arc 1: Exit



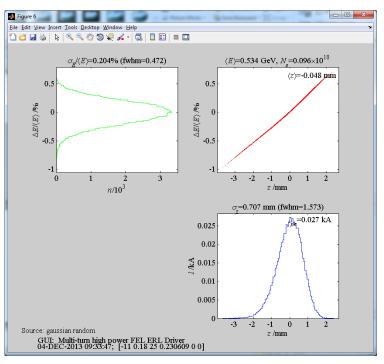
Linac 2: Exit Pass 1



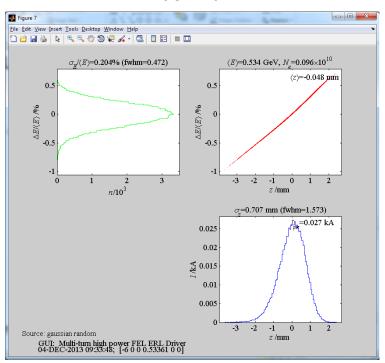
Arc 2: Exit



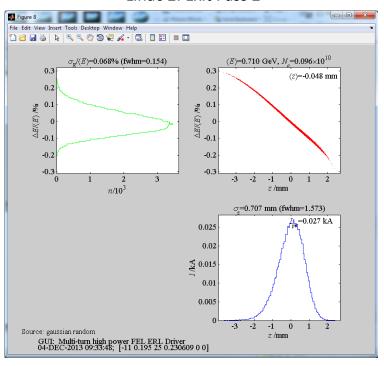
Linac 1: Exit Pass 2



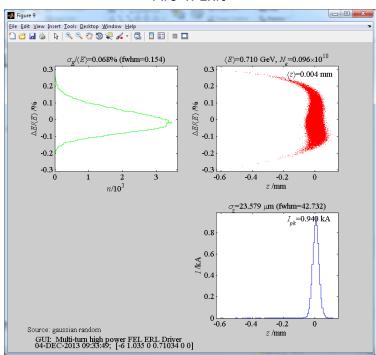
Arc 3: Exit



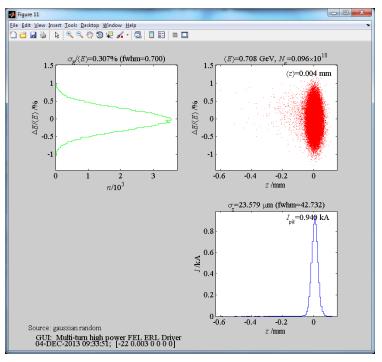
Linac 2: Exit Pass 2



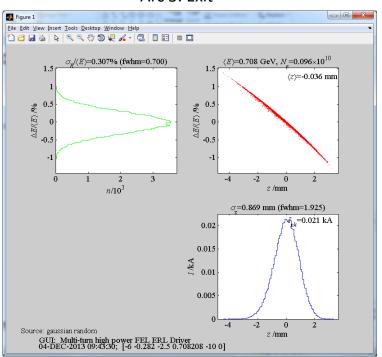
Arc 4: Exit



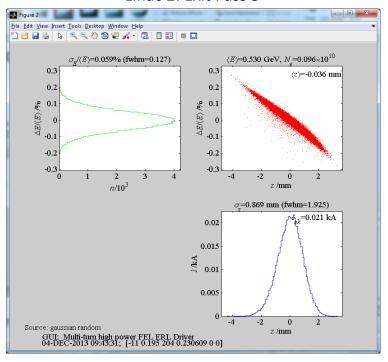
After FEL



Arc 5: Exit

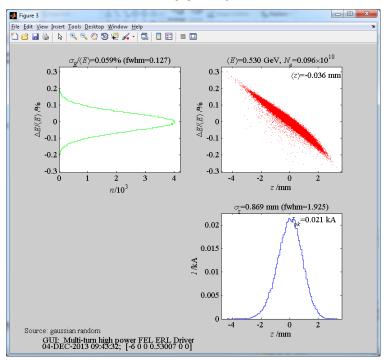


Linac 2: Exit Pass 3

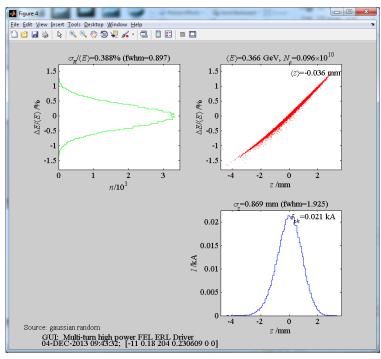


Longitudinal Phase Space

Arc 6: Exit

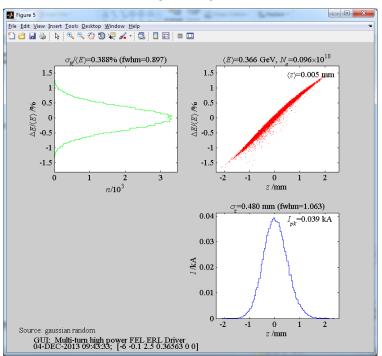


Linac 1: Exit Pass 3

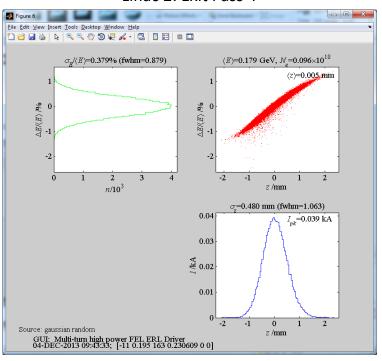


Longitudinal Phase Space

Arc 7: Exit

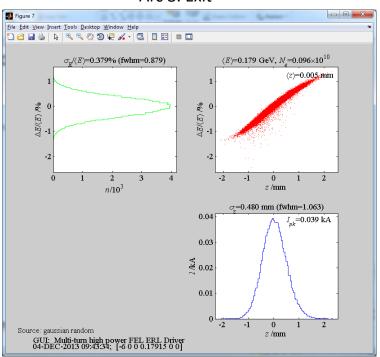


Linac 2: Exit Pass 4

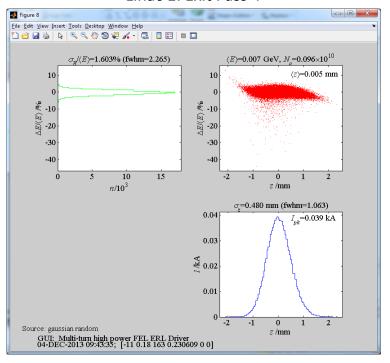


Longitudinal Phase Space

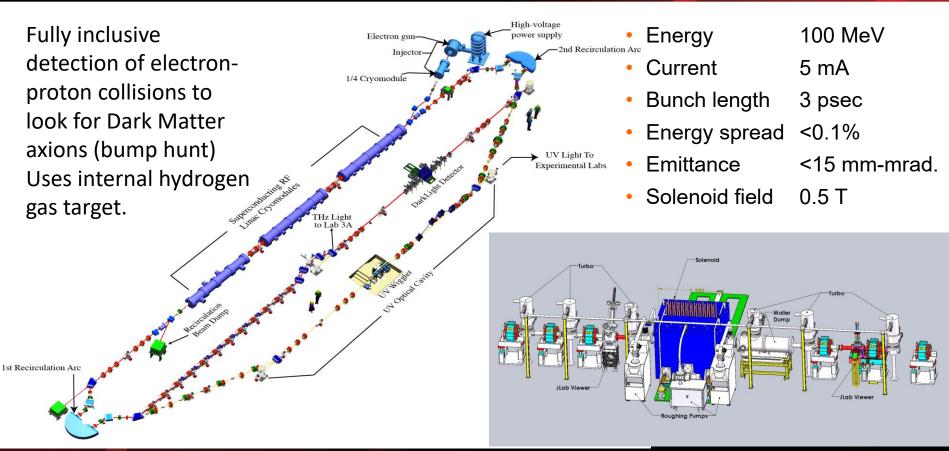
Arc 8: Exit



Linac 1: Exit Pass 4

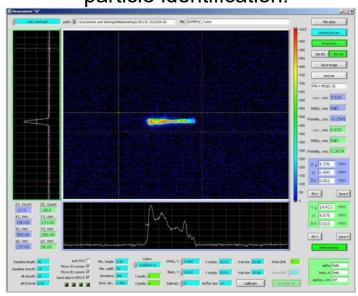


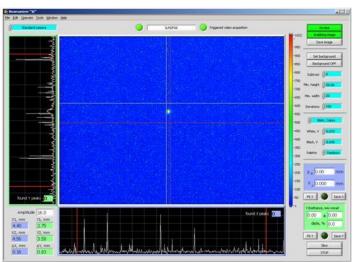
DarkLight Experiment



- Bunch is no longer compressed at the target.
- Energy spread is very small, thus insensitive to multipoles.

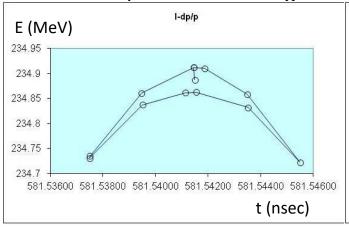
 Desire fo low repetition rate to take advantage of time-of-flight in particle identification.

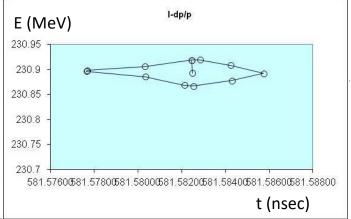




- Bunch is no longer compressed at the target.
- Energy spread is very small, thus insensitive to multipoles.
- Desire fo low repetition rate to take advantage of time-of-flight in particle identification.
- Can switch between quite different operational modes with only minor parametric changes
 - e.g. cross-phasing of linac cavities/modules: change single phase setpoint and go from short bunch to small dp/p
- Can use short bunch setup to optimize longitudinal transfer map.
- Can use two-pass setup to have very small energy spread.
- Note: Thompson backscattering requires high charge with moderately short bunches. This setup could be very advantageous for that application as well.

- Bunch is no longer compressed at the target.
- Energy spread is very small, thus insensitive to multipoles.
- Desire fo low repetition rate to take advantage of time-of-flight in particle identification.
- Can switch between quite different operational modes with only minor parametric changes

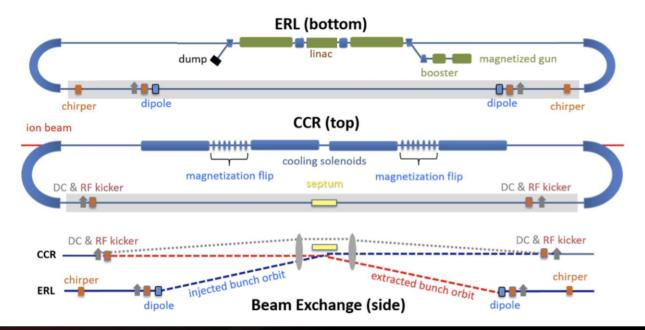




- Bunch is no longer compressed at the target.
- Energy spread is very small, thus insensitive to multipoles.
- Desire fo low repetition rate to take advantage of time-of-flight in particle identification.
- Can switch between quite different operational modes with only minor parametric changes
 - e.g. cross-phasing of linac cavities/modules: change single phase setpoint and go from short bunch to small dp/p
- Can use short bunch setup to optimize longitudinal transfer map.
- Can use two-pass setup to have very small energy spread.
- Note: Thompson backscattering requires high charge with moderately short bunches. This setup could be very advantageous for that application as well.

EIC Cooler ERL and CCR

- Need very long, small energy spread bunch with very high charge.
- Magnetized electron beam for higher cooling efficiency
- Repetition rate of bunches is 476.3 MHz.
- Assume high charge, low rep-rate injector (w/ harmonic linearizer acceleration)





JLEIC BBU Cooler Specifications

• Energy 20–110 MeV

• Charge 3.2 nC

CCR pulse frequency 476.3 MHz

• Gun frequency 43.3 MHz

• *rms* Energy spread (uncorr.) 3x10⁻⁴

• Energy spread (p-p corr.) <6x10⁻⁴

Bunch length (tophat)
 3 cm (17°)

Thermal (Larmor) emittance
 <19 mm-mrad

Cathode spot radius 3.1 mm

Cathode field 0.05 T

Normalized hor. drift emittance 36 mm-mrad

Solenoid field 1 T

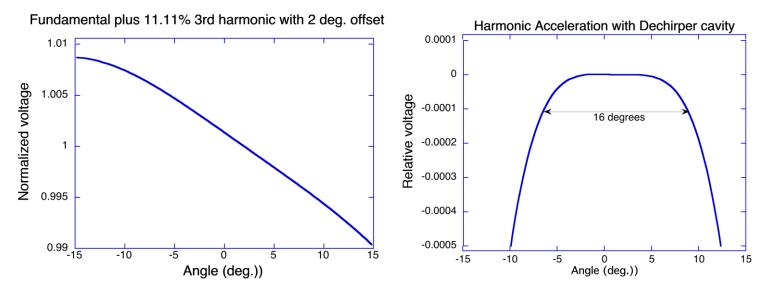
• Electron beta in cooler 37.6 cm

Solenoid length 4x15 m

• Bunch shape beer can

Voltage with 3rd Harmonic and phase and amplitude offsets

• If we want to accelerate a very long bunch and then stretch it out even more we can use 3rd harmonic cavities in the linac.



Before going into the CCR, take out the slope using a 952.6 MHz de-chirper. We can also put in a quartic correction if necessary by changing the amplitude

Conclusions

- ERL architecture is determined by the longitudinal design.
- Transverse design follows the longitudinal settings.
- For FELs one wants a high peak current:
 - For small long wavelengths a parallel to point focus is optimal
 - For short wavelengths a telescopic focus is better.
- Nuclear Physics applications do not need high peak current but need small relative energy spread.
 - Can use either lattice of harmonic RF to get a good energy spread
 - Low charge, high repetition rate is a better match to these applications.
- Electron Cooling applications need extremely long bunches and extremely small energy spread.
 - Harmonic RF is almost required for such bunches.
 - Microbunching and CSR are now the big challenges.



Compaction Management

LINAC	Energy Gain (MV)	Phase (Deg)	ARC	M ₅₆ (m)	T ₅₆₆ (m)	W ₅₆₆₆ (m)
1	0.1800	-16	1	0	0	0
2	0.1950	-16	2	-0.0295	-1.23	-9
3	0.1800	+25	3	0	0	0
4	0.1950	+25	4	+1.035	0	0
5	0.1950	204	5	-0.282	-2.5	-10
6	0.1800	204	6	0	0	0
7	0.1950	163	7	-0.1	+2.5	0
8	0.1800	163	8	0	0	0

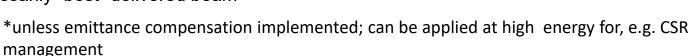


ERLs are time-of-flight spectrometers

- Exist solely to create conspiracies between phase and energy
 - no closed orbit; may not be betatron stable/have "matched" beam envelopes ⇒ beam and lattice are different (mismatch often advantageous)
 - longitudinal match constrains system architecture
- need full suite of *longitudinal* diagnostics for both machine (lattice) and beam
 - phase transfer function system (M₅₅, T₅₅₅)
 - bunch length monitoring/noninvasive energy spread
 - tomography to capture/correct nonlinear phase space distortion
- spectrometer-grade components
 - perturbations at high energy anti-damp during recovery
- aberration management critical: nonlinear modeling/diagnosis/control needed

Features of ERL Architectures (cont.)

- no equilibrium ⇒ stability a challenge
 - CEBAF parity-quality beam provides benchmark
- high beam power, absence of equilibrium ⇒ CW is a gamechanger
 - beam loss monitoring/suppression
- beam quality generation and preservation:
 - beam quality declines from cathode onward*; "best" injected beam not necessarily "best" delivered beam



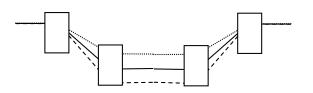
- beam degrades at full energy ⇒ anti-damping makes things worse during recovery
- Recirculator/ERL ⇒ multiple beams/common transport (at least in linac!)
 - creates challenges for monitoring & control



Bates band - design by Sargent/Flanz from MIT (combined function magnets)

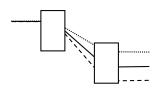
J. B. Flanz and C. P. Sargent, "Operation of an Isochronous Beam Recirculation System," *Nucl. Instrum.* and *Methods* **A241** (1985) 325–333

D. Douglas separated sextupoles and added quads



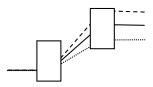


Bates band - design by Sargent/Flanz from MIT (combined function magnets)



J. B. Flanz and C. P. Sargent, "Operation of an Isochronous Beam Recirculation System," *Nucl. Instrum. and Methods* **A241** (1985) 325–333

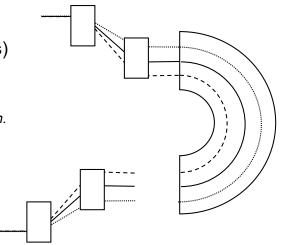
D. Douglas separated sextupoles and added quads



Bates band - design by Sargent/Flanz from MIT (combined function magnets)

J. B. Flanz and C. P. Sargent, "Operation of an Isochronous Beam Recirculation System," *Nucl. Instrum.* and *Methods* **A241** (1985) 325–333

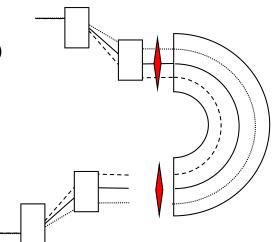
D. Douglas separated sextupoles and added quads



Bates band - design by Sargent/Flanz from MIT (combined function magnets)

J. B. Flanz and C. P. Sargent, "Operation of an Isochronous Beam Recirculation System," *Nucl. Instrum. and Methods* **A241** (1985) 325–333

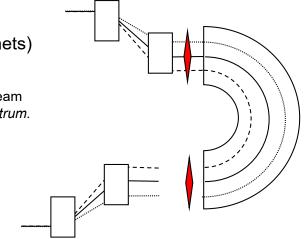
D. Douglas separated sextupoles and added quads



Bates band - design by Sargent/Flanz from MIT (combined function magnets)

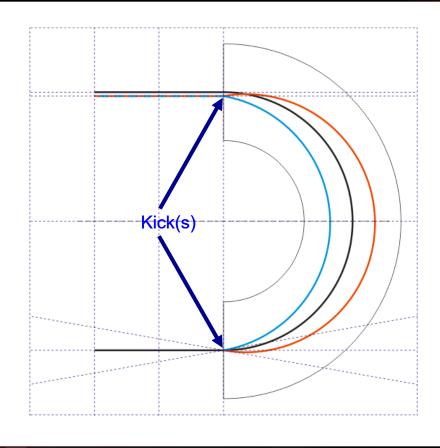
J. B. Flanz and C. P. Sargent, "Operation of an Isochronous Beam Recirculation System," *Nucl. Instrum. and Methods* **A241** (1985) 325–333

D. Douglas separated sextupoles and added quads



- Really robust
- Really easy to operate (if it is instrumented)
- Really simple (<u>if</u> you think about it the right way)
- Good acceptance (>10% energy, 30-40 deg phase)
- Symmetry aberrations corrections
- Match in/out with chromatically balanced telescopes

180° Bates bend (1)

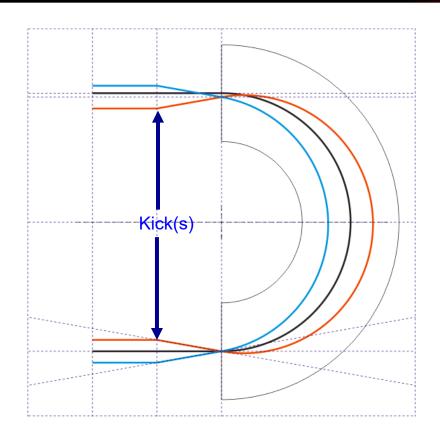


Path length change with kick;

$$\delta L = 2\rho \, \delta x'$$

Used to adjust the path length i.e. phase of the energy recovered beam

180° Bates bend (2)



Path length change with kick;

$$\delta L = 2\rho \, \delta x'$$

Kick by quadrupole;

$$\delta x'(x) = A \cdot x$$

Kick by sextupole;

$$\delta x'(x) = B \cdot x^2$$

Due to dispersion created by first two dipoles;

$$E \propto x$$