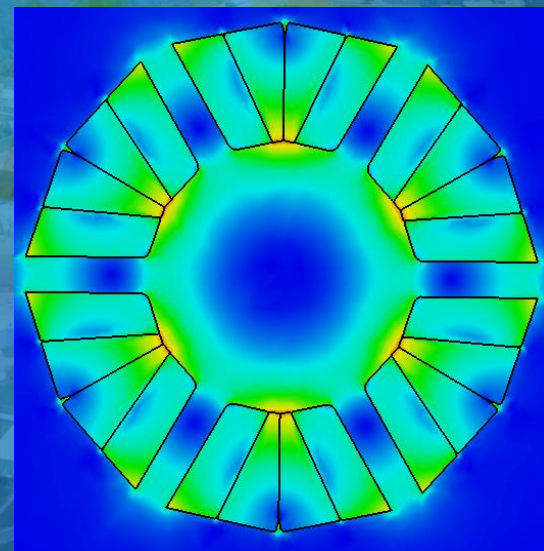


SEPTEMBER 17, 2024

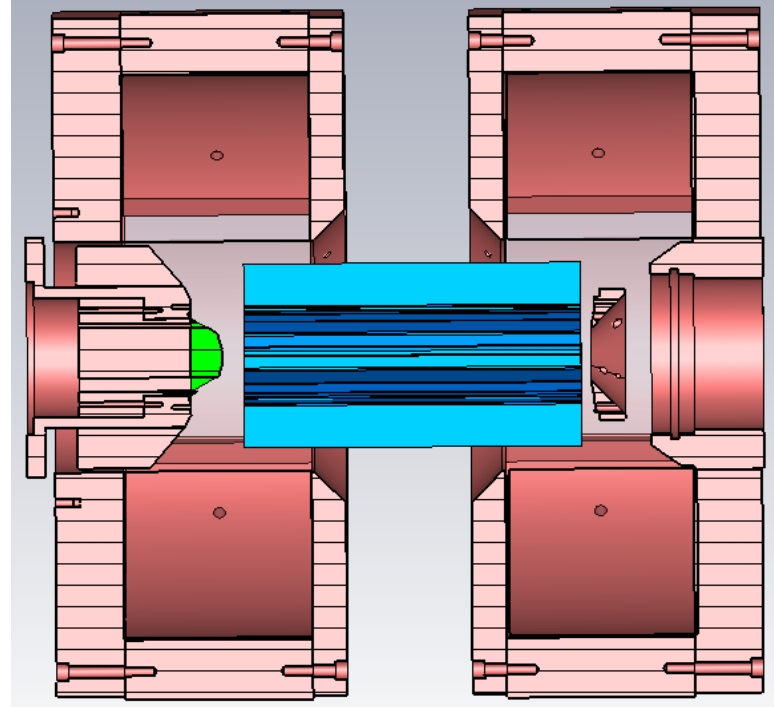
ECR2 PERFORMANCE UPGRADES AT ATLAS



JAKE MCLAIN
Ion Source Engineer

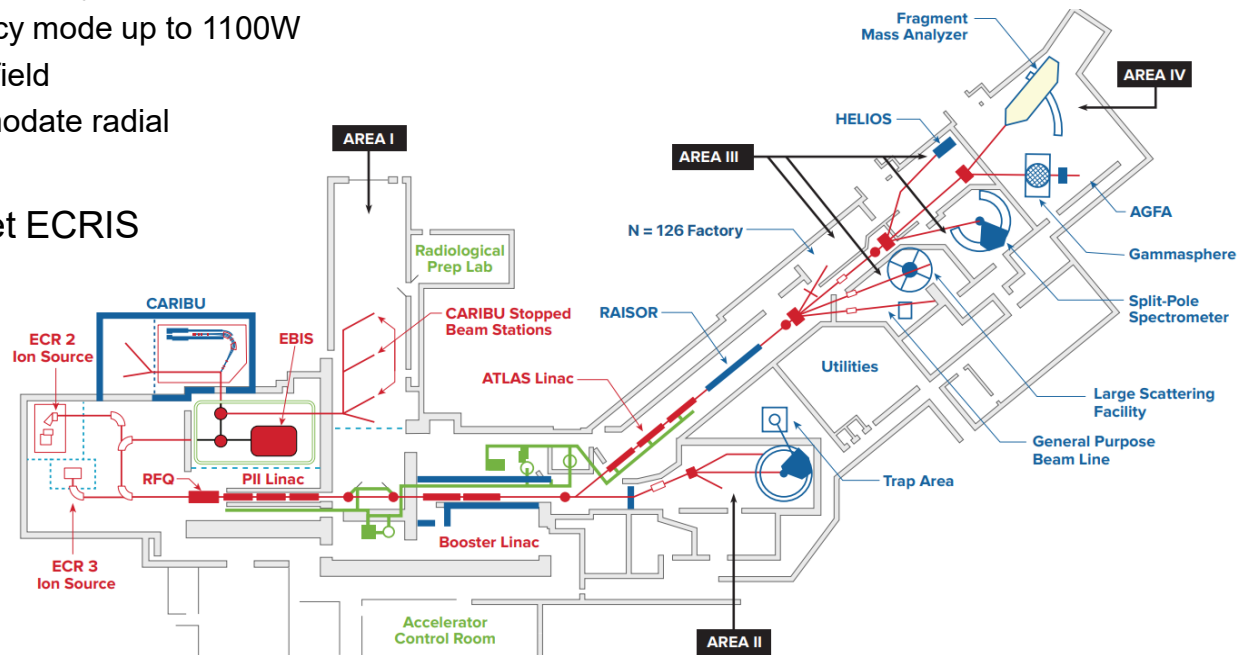
OUTLINE

- History and Current Performance
- Upgrade Motivation
- 18GHz ECR2
- Magnetic Improvements
 - Hexapole Upgrade
 - Axial Field Upgrades
- Plasma Chamber Redesign
- Supporting Hardware Redesign
- Extraction Optics
- Expected Performance



ATLAS ECR ION SOURCES

- The Argonne Tandem Linac Accelerator System (ATLAS) has two ECR ion sources, ECR2 and ECR3.
- ECR2 is a room temperature AECS style ECRIS
 - Typically run in a multiple frequency mode up to 1100W
 - 2 solenoid magnets provide axial field
 - Open hexapole design to accommodate radial material introduction and pumping
- ECR3 is an all-permanent magnet ECRIS
 - Formerly the BIE100
 - Used primarily for ^{14}C and gases
- ECR2 is the workhorse ion source at ATLAS



ECR2 HISTORY AND PERFORMANCE

Are we due for an upgrade?

- Currently running well, but not well enough for the facility requirements moving forward
 - N=126 Factory being commissioned
- ECR2 was originally built in 1997
 - Designed for 10GHz & 14GHz 2-frequency operation
- Hexapole and injection iron upgrade in 2003
 - Raised injection B field to 2.0 T from 1.7 T
 - Raised wall B field to 0.98 T from 0.85 T
 - NdFeB magnet material and design improvements
 - Still fell short of the ideal 1.1T B_{rad} for 14GHz operation
 - Roughly a factor of 2 increase in beam intensities



IMPROVING FACILITY CAPABILITIES

Why upgrade a well functioning source?

- Upcoming ATLAS experimental campaigns require increase in intensity capabilities from ECR2
 - Typically, middle to high charge state requirements
 - Table assumes 60% source to target. 40% is typical.
- Upgrade must retain room temperature designs
 - Improve hexapole design
 - Consider different permanent magnet materials
 - Improve injection iron design
- Optimize 14GHz and support 18GHz operation
 - Most other facilities' 18GHz improvement results are sufficient for our intensity goals

Beam Species	Current Performance	Desired Performance
Ca-48	2puA	2puA
Ti-50	0.9puA	1puA
Xe-136	0.7puA	5puA
U-238	<0.1puA	1puA

SCALING LAWS FOR 18 GHZ ECR2

What needs to change?

- Scaling laws for performance have driven design decisions

- $I_{peak} \propto f_{RF}^2$

- $\frac{B_{rad}}{B_{ECR}} = 2$

- $\frac{B_{inj}}{B_{ECR}} = 4$

- $V_{ext} \propto I_{tot}^{2/3} \propto f_{RF}^{4/3}$

Frequency	∇B_{ECR}	B_{min}/B_{ECR}
14.5 GHz	5.87	0.695
18 GHz	7.45	0.560

- Must preserve appropriate magnetic gradients at the resonant surface to avoid plasma instabilities
 - ∇B_{ECR} greater than 5.8 T/m and a B_{min}/B_{ECR} less than 0.7
 - Fully adjustable solenoid magnets to dial in fields and stability

HEXAPOLE

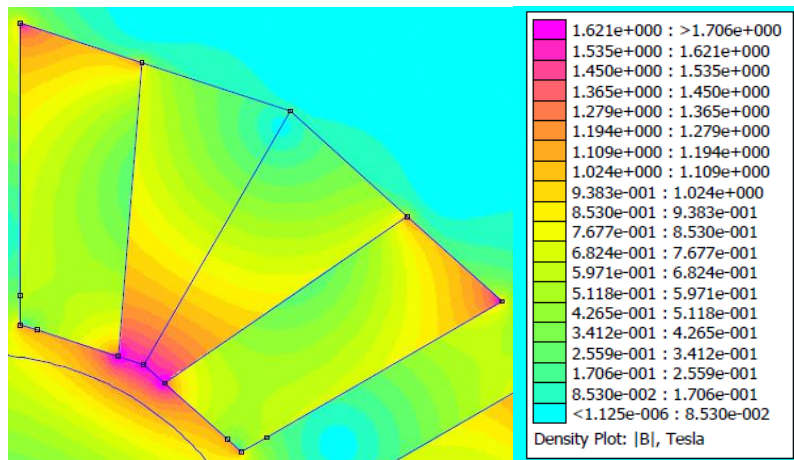
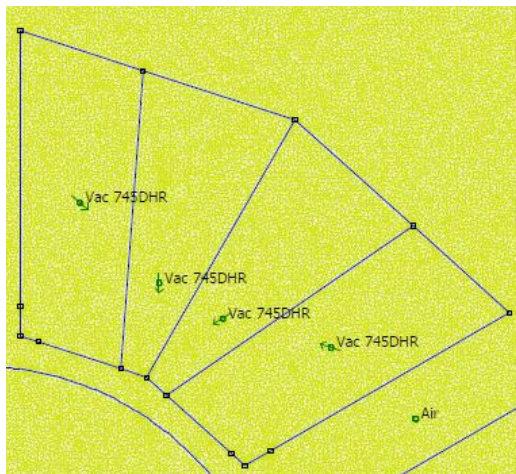
What permanent magnet material?

- ECR2 presently uses MCE N5064
- Originally down to two choices
 - Vacodym 745 DHR & MCE N5064
- Main factors for material consideration
 - High H_{cB} (coercivity) for high B field
 - High H_{cJ} (intrinsic coercivity) to resist demagnetization
 - High temperature resistance
- We later found that Vacodym 745 DHR is a surface treatment of Vacodym 745 HR
- How does Vacodym 745 HR perform?
 - Bulk material available
 - Highest coercivity among the materials discussed
 - Consider the DHR treatment if demagnetization is a large concern after simulations

Material	$H_{cB,min}$ (kA/m)	$H_{cJ,min}$ (kA/m)
Vac 745 DHR (2mm depth)	1046	1631
Vac 745 HR	1065	1115
MCE N5064	1050	1114

MAXIMIZE B_{rad} AND AVOID DEMAGNETIZATION

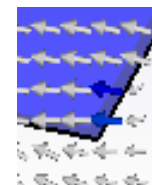
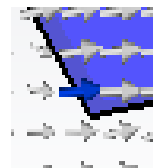
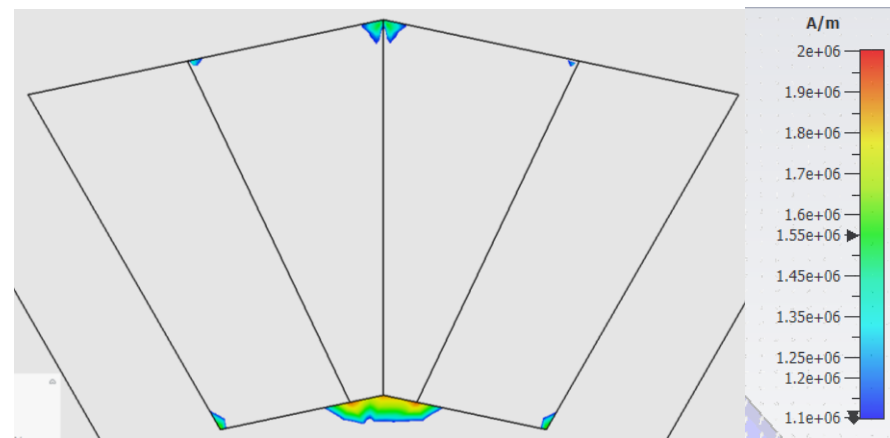
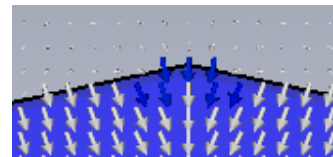
- Many iterations of magnet shapes and magnetization vectors considered
- Best design utilized 4 segments per magnet bar
- 2D simulations in FEMM resulted in a B_{rad} of 1.22T
- This design was then exported to CST for 3D simulations
 - First without contributions from the solenoid magnets, then with them
 - Finally analyze the demagnetization potential of the magnets



2024 HEXAPOLE

3D *without* solenoid magnet contributions

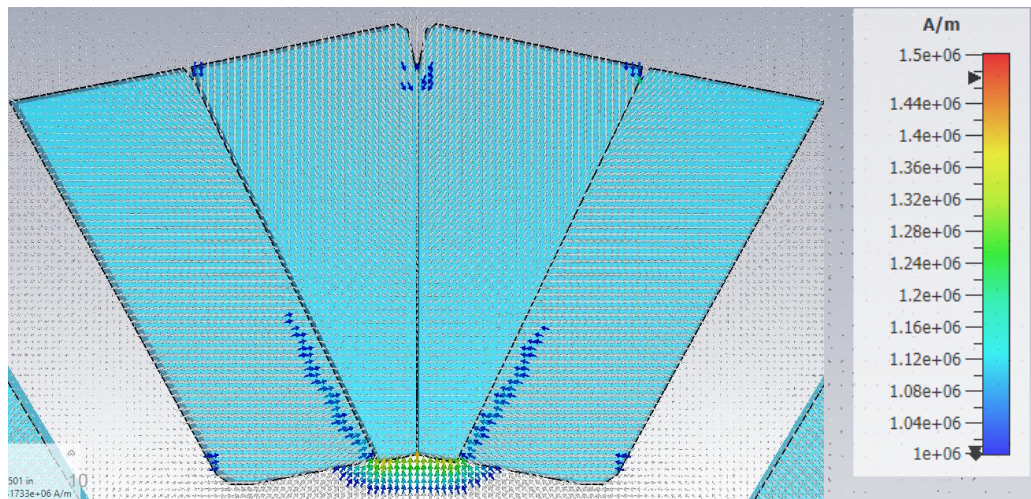
- $B_{\text{rad}} = 1.19 \text{ T}$ at source midplane
- Running the 3D simulation for the magnet bars without solenoid contributions exposed potential problem areas
 - Color on plot indicates $>1100 \text{ kA/m}$
 - Arrows show direction of field primarily against magnetization angle
- Next, simulate “effective” geometry with removed demagnetized sections
 - Solenoid H field contributions will only make things worse for demagnetization
 - Cut out expected demagnetized sections of magnet bar
 - » Assumed to not contribute to the field



2024 HEXAPOLE

3D *without* solenoid magnet contributions

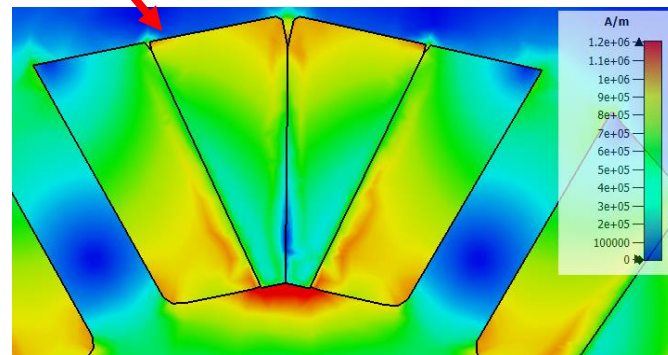
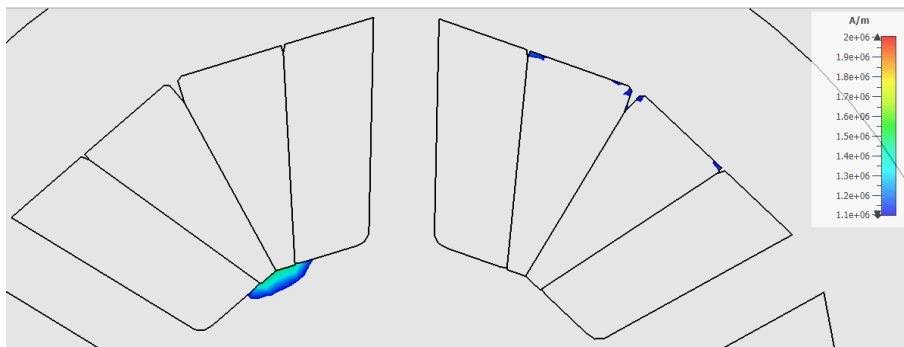
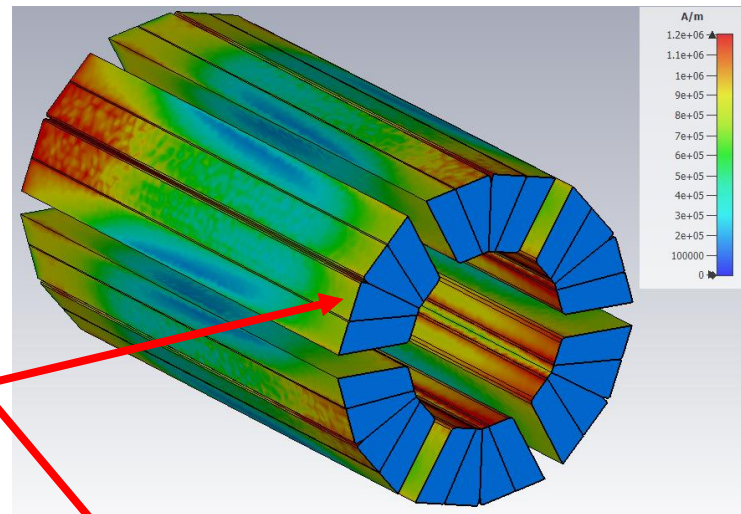
- Second iteration
 - No demagnetization field with chamfers added throughout the problem areas of magnet
- $B_{\text{rad}} = 1.17 \text{ T}$ at source midplane
- Maximum H field less than $1.1\text{E}6 \text{ A/m}$
- No need to do additional cut outs
 - Onto the 3D model with solenoid contribution
 - Will confirm with additional simulation that demagnetizing field does not exceed $1.1\text{E}6 \text{ A/m}$



2024 HEXAPOLE

3D with solenoid magnet contributions

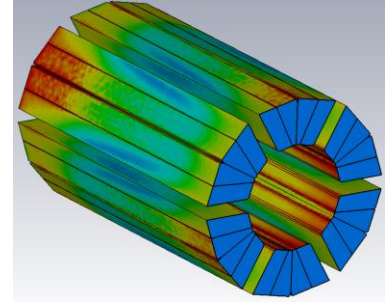
- Simulated new hexapole with injection and extraction solenoids at 525A
 - $B_{\text{rad}} = 1.18\text{T}$ at source midplane
- Took H field slice at max H field axial position
 - Portions of magnet are over $1.1\text{E}6\text{ A/m}$
 - Must look at demagnetization field against magnetization angle



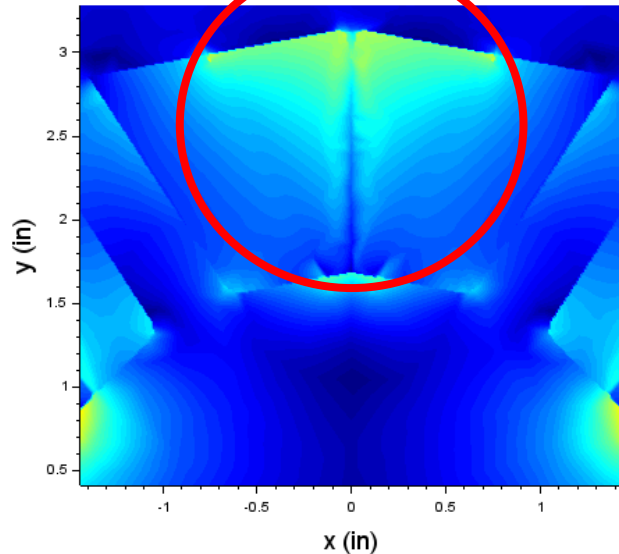
2024 HEXAPOLE

3D with solenoid magnet contributions

- Maximum H field along the demagnetization vector is $1.10\text{E}6$ A/m
 - $H_{\text{CJ,min}}$ is $1.15\text{E}6$ A/m
 - This is under, but barely under, where demagnetization occurs at room temperature
 - Will carry out the diffusion treatment to give us the temperature and demagnetization capabilities of the 745 DHR in the concerning areas near the surface of the magnet bar

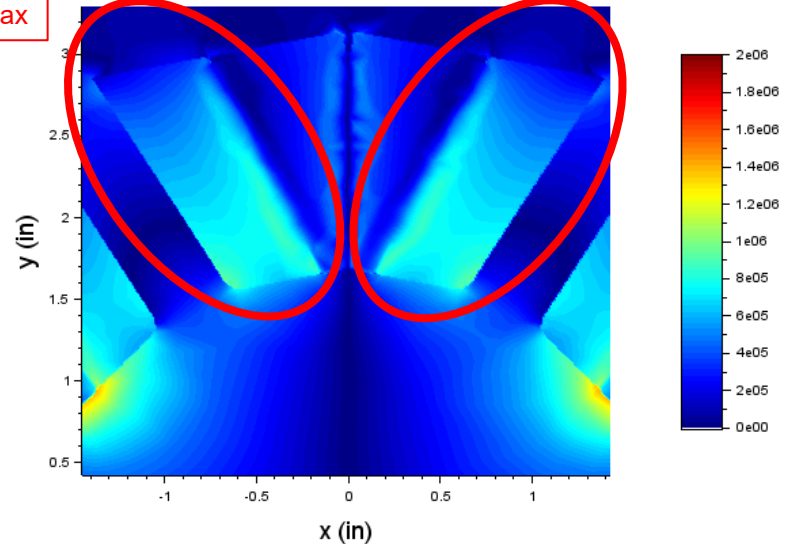


H projection onto one magnet segments magnetization angle



1.10E6 A/m max

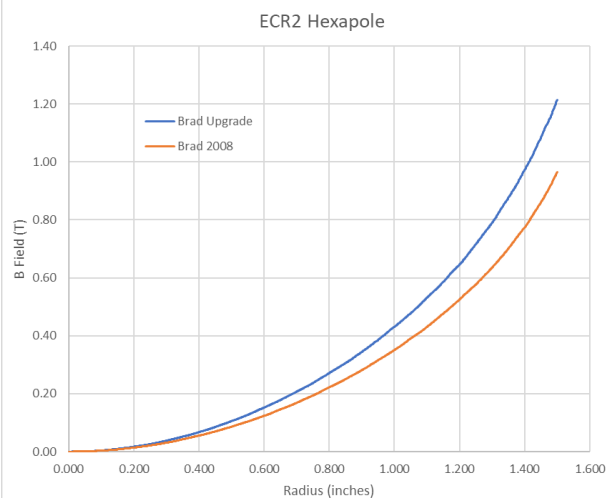
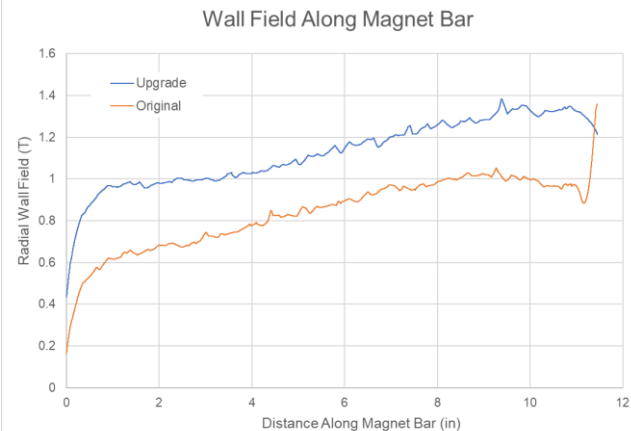
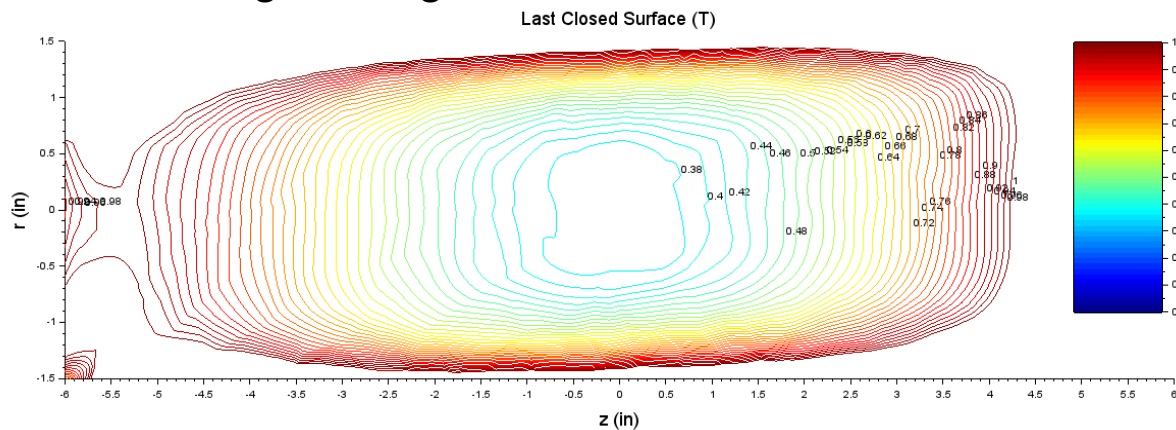
H projection onto one magnet segments magnetization angle



2024 HEXAPOLE

3D with solenoid magnet contributions

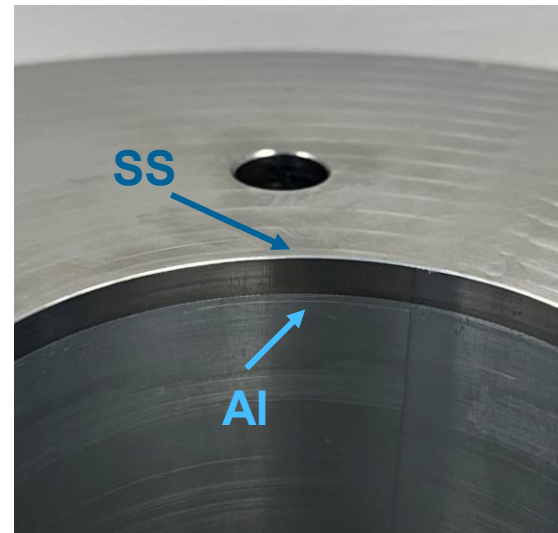
- Last closed surface $\sim 1.0\text{T}$
 - Was 0.85T before upgrade
- Large improvement over current hexapole
- Added bonuses of temperature resistance and demagnetizing field resistance



NEW PLASMA CHAMBER

Some old, some new designs incorporated

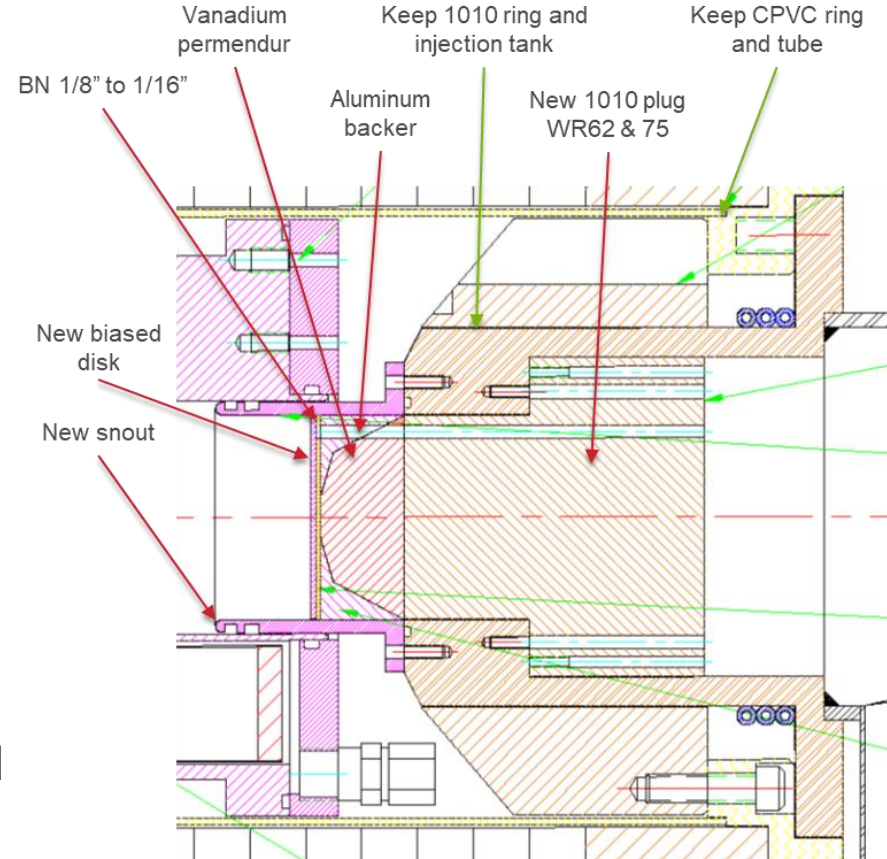
- Expand OD to accommodate new design
 - 0.5-inch increase for larger magnets
- Aluminum and SS bulk material
 - Explosion bonded/welded together
 - Al portion where plasma and heat load are located
 - SS portion where multiple welds are needed
 - SS on extraction side
 - Issue with consistent weld quality when using only aluminum (leaks)
- Cover plate
 - maintain current OD
 - Remove some previously used o-rings and replace them with screws that have integrated o-rings



NEW INJECTION IRON DESIGN

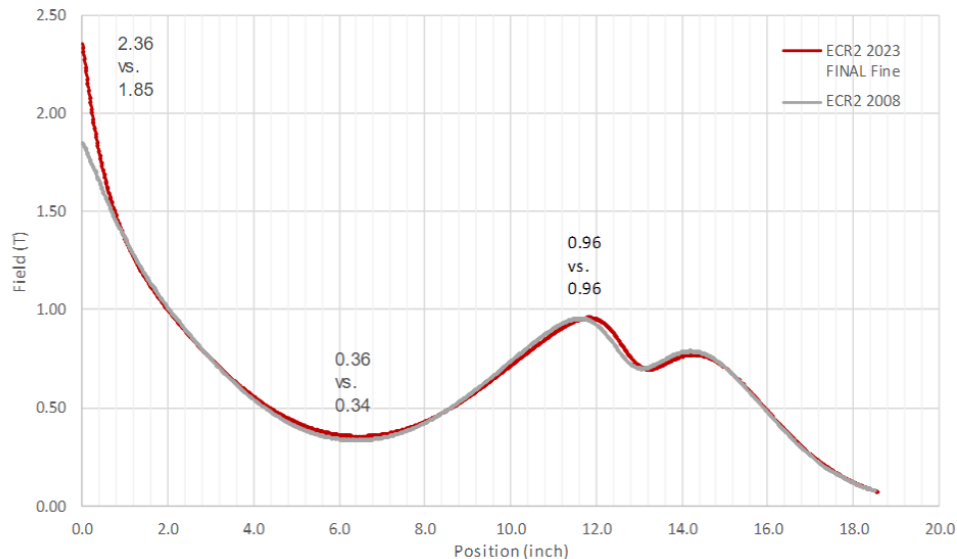
Novel materials help

- Addition of Vanadium Permendur on injection iron
 - Cobalt-iron alloy with small % vanadium
 - High saturation
 - High permeability
- Rework the injection iron for WR62 and WR75 only
- Leaves room for a thinner but still adequate BN insulator between the biased disk and injection iron
- This greatly improves the injection field



SUPPORTING UPGRADES

- Need to revise high voltage insulation throughout
 - Last slide showed injection adjustments
- Requires new extraction electrode
- Requires revision to 1010 steel in extraction region
- Requires higher voltage extraction to support increased intensity
- Requires magnet cooling upgrade
 - New DI water skid
- Must look at ion optics of the immediately downstream low energy beam transport line



ION OPTICS

Pre-upgrade conditions

- 14kV Extraction
- 100uA 16/4+
- -1kV Puller
- Solenoids and Glaser contributions
- 100% transmission to faraday cup downstream of analyzing magnet
- This configuration is not sufficient for increased intensities of the upgrade

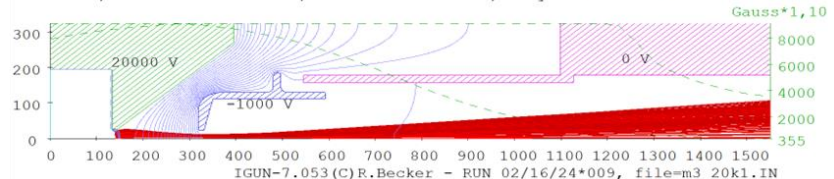


ION OPTICS

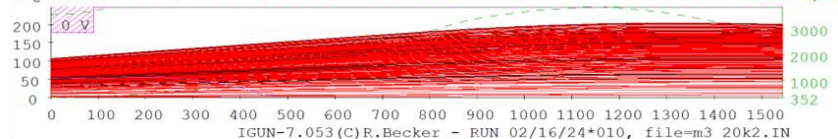
2024 Upgrade

- 14kV Extraction, 1mA 16/4+
- -1kV Puller
- 525A Solenoids and Glaser contributions
- Added in new einzel lens
 - 81% transmission without einzel lens
- Beam lost after dipole magnet in drift region (space charge effects)
- 100% transmission to FCF101 with new einzel lens before dipole magnet
- Successfully simulated up to 20kV extraction and 3mA at 100% transmission to FCF101

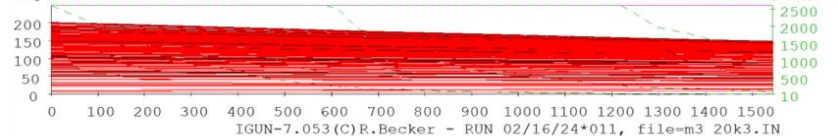
Up=20012.9, Te=3.0 eV, Ui=5.0 eV, mass=16.0, Ti=1.0 eV, Usput=0 V
 2.94E-3 A, crossover at Z= 387, R=11.66 mesh units, Debye=0.301 mesh units



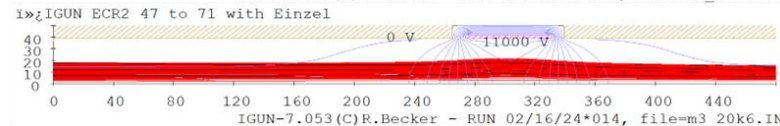
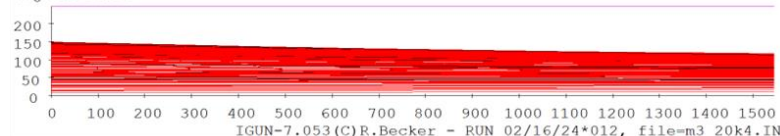
2.98E-3 A, crossover at Z= 1, R=106.95 mesh units
 I>IGUN ECR2 220A Glazer



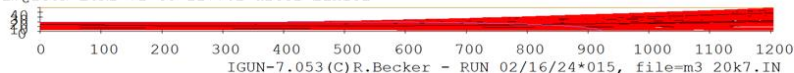
2.98E-3 A, crossover at Z= 1544, R=148.27 mesh units
 I>IGUN ECR2 220A Glazer



2.98E-3 A, crossover at Z= 1544, R=117.04 mesh units
 I>IGUN ECR2



2.98E-3 A, crossover at Z= 199, R=18.42 mesh units
 I>IGUN ECR2 71 to 117.61 after Einzel



2024 ECR2 SUMMARY & EXPECTATIONS

- ECR2 at ATLAS is due for an upgrade and beam intensity requests are increasing
- An upgrade plan to support 18GHz operation has been established and approved
- A new hexapole was designed and simulated for performance and demagnetization
- A new plasma chamber was designed for the new hexapole magnet bars
- Iron and vanadium permendur components were designed to maximize axial B field
- Ion optics simulations were completed, demonstrating the need of an einzel lens for high intensities

Parameter	Current	Upgrade
B_{inj}	1.85 T	2.44 T
B_{min}	0.34 T	0.36 T
B_{ext}	0.96 T	1.00 T
B_{last}	0.85 T	1.00 T
Coil currents	500 / 500 A	525 / 525 A
B_{rad}	0.96 T	1.18 T
Plasma chamber radius	38.1 mm	38.1 mm
Plasma chamber length	297 mm	297 mm
Hexapole inner radius	42.4 mm	42.4 mm
Hexapole outer radius	74.7 mm	79.7 mm