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# Ultralow Emittance Light Sources

Particle Accelerator Conference  
Genova, Italy

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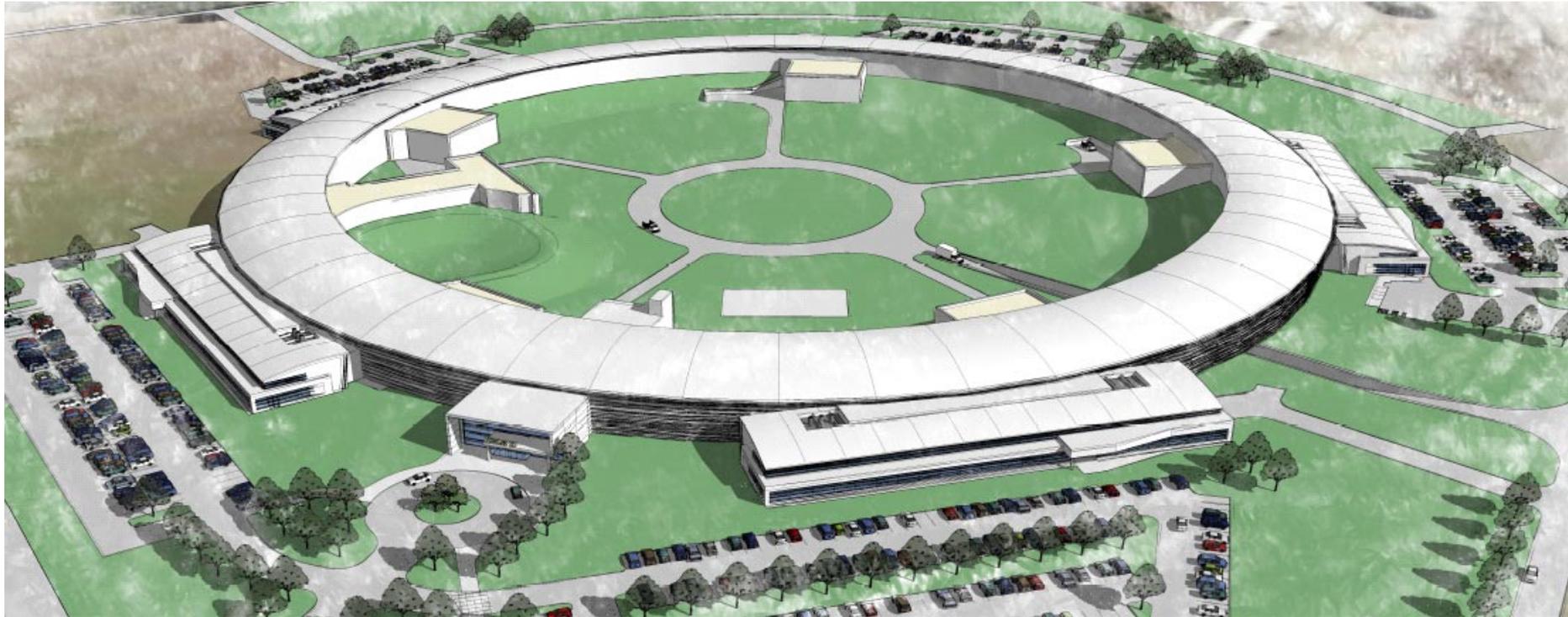
Johan Bengtsson for the NSLS-II Design Team

# Outline

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- **Challenges**
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# The Facility



# Acknowledgements

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# What's Known

- Dedicated third generation light sources: ~20 years of optimizations.
- The horizontal emittance (isomagnetic lattice) is given by

$$\varepsilon_x \text{ [nm}\cdot\text{rad]} = 7.84 \times 10^3 \cdot \frac{(E \text{ [GeV]})^2 F}{J_x N_b^3}$$

$N_b$  is the number of dipoles,  $0 < J_x < 3$ ,  $F \geq 1$ . No dipole gradients  $\Rightarrow J_x \approx 1$ .

- Generalized Chasman-Green Lattices: DBA, TBA, QBA, 7-BA [1].
- Effective emittance  $\Rightarrow$  chromatic cells.
- Increasing  $N_b$  reduces  $\varepsilon_x$  but also reduces peak dispersion, which makes the chromatic correction less effective  $\Rightarrow$  “chromaticity wall” [2].
- Damping wigglers (DWs): damping rings and conversion of HEP accelerators [3,4].
- Mini-Gap Undulators (MGUs), Three-Pole-Wigglers (TPWs) inside DBA [5].

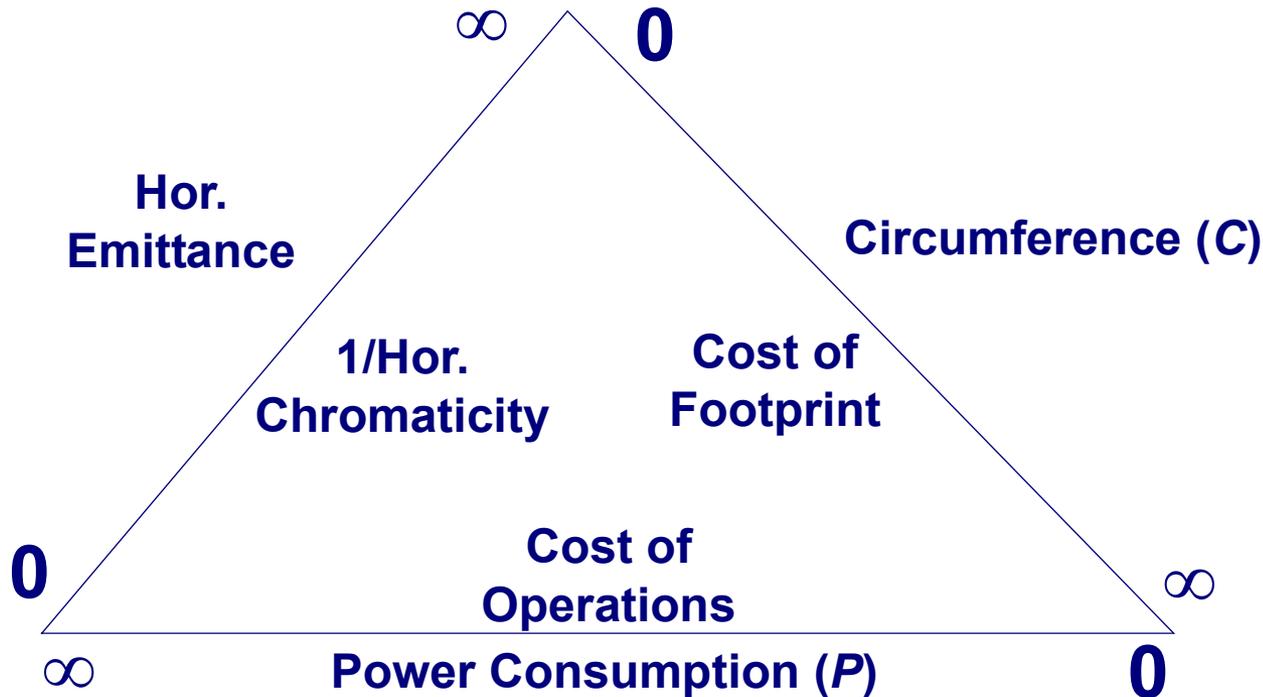
# What's New

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- Use of damping wigglers to reduce horizontal emittance and as high flux X-ray sources => achromatic cells and weak dipoles.
- Medium energy ring (3 GeV) with ~30 DBA cells.
- Vertical orbit stability requirements.
- Generalized higher order achromat.

# Global Optimization

1. Horizontal emittance (natural): damping  $\leftrightarrow$  diffusion (fundamental limit is IBS).
2. Optimize (for Insertion Devices (IDs)) [6]:



$$\varepsilon_x \sim \frac{1}{R^2 \cdot P}$$

$R$  bend radius

# Challenges

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## Non-linear dynamics:

- **Medium energy: control of Touschek life time and momentum aperture.**
- **30 DBA cells: control of tune footprint.**
- **Control of impact of DWs and IDs: include leading order nonlinear effects from DWs in Dynamic Aperture (DA) optimizations.**
- **Optics requirements for IDs and top-up injection: introduce alternating straights with high- and low horizontal beta function  $\leftrightarrow$  reduced symmetry (30  $\rightarrow$  15).**
- **DBA: momentum dependence of optics functions  $\Rightarrow$  number of chromatic sextupole families.**

## Technical

- **Weak dipoles: introduce TPWs (adjacent to the dipoles)  $\Rightarrow$  control of peak beta functions and horizontal dispersion.**
- **Vertical orbit stability: sub micron  $\Rightarrow$  pushing the state-of-the-arts [7,8].**

# Lattice Parameters

<b>Energy</b>	<b>3 GeV</b>
<b>Circumference</b>	<b>791.5 m</b>
<b>Beam Current (<math>I_b</math>)</b>	<b>500 mA</b>
<b>Bending Radius (<math>R</math>)</b>	<b>25.0 m</b>
<b>Dipole Energy Loss (<math>U_0</math>)</b>	<b>286.5 keV</b>
<b>Emittance (<math>\varepsilon_x, \varepsilon_y</math>): bare/w. 8 DWs</b>	<b>(2.1, 0.01)/(0.6, 0.01) nm·rad</b>
<b>Momentum compaction</b>	<b>0.00037</b>
<b>RMS Energy Spread: bare/w. 8 DWs</b>	<b>0.05/0.1%</b>
<b>Working point (<math>\nu_x, \nu_y</math>)</b>	<b>(32.4, 16.3)</b>
<b>Chromaticity (<math>\xi_x, \xi_y</math>)</b>	<b>(-100, -42)</b>
<b>Peak Dispersion (<math>\hat{\eta}_x</math>)</b>	<b>0.45 m</b>
<b>Beta Function (<math>\beta_x, \beta_y</math>): long/short straight</b>	<b>(18, 3)/(3, 3) m</b>

# Intrabeam Scattering (IBS)

## Equilibrium

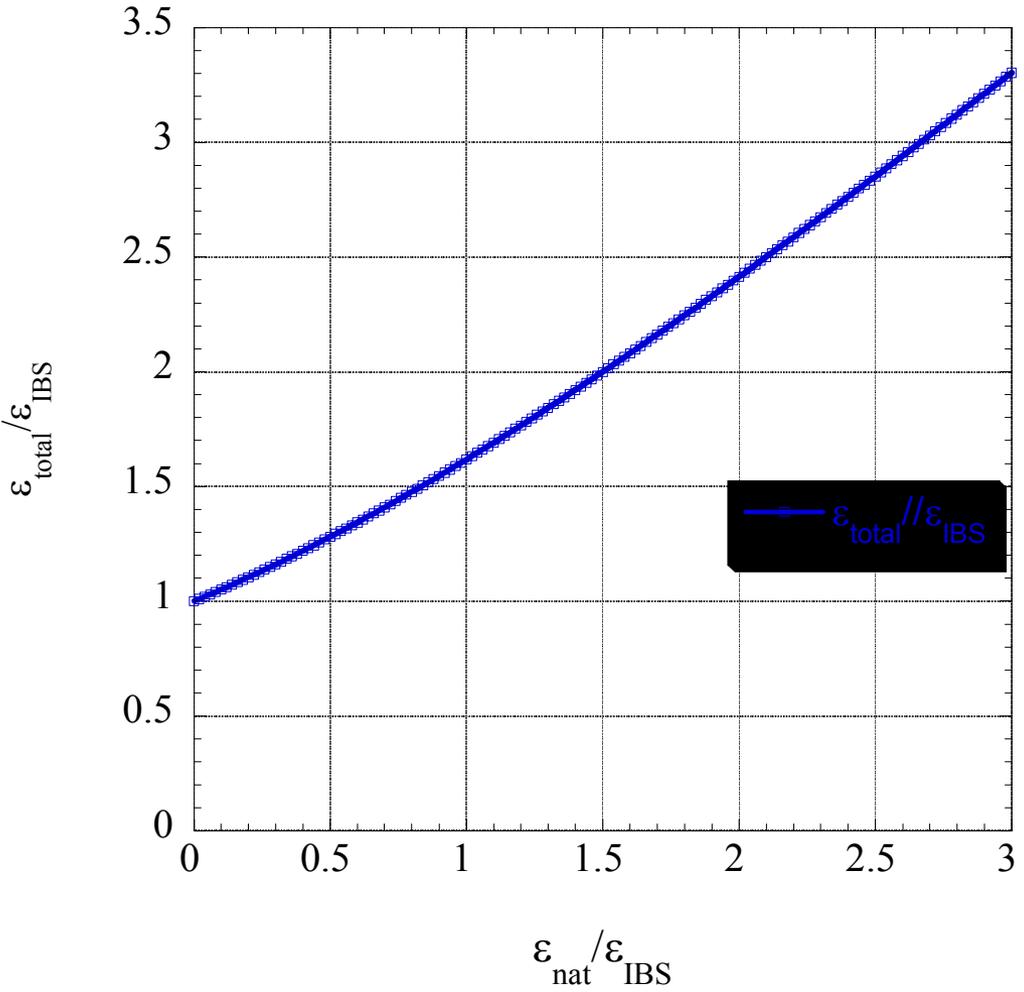
$$\varepsilon_{\mathbf{x}} = \varepsilon_{\mathbf{x}}^{\text{SR}} + \varepsilon_{\mathbf{x}}^{\text{IBS}} = \tau_{\mathbf{x}}(\mathbf{E}^{\text{SR}}) \langle \mathcal{H} \cdot (\mathbf{D}_{\delta}^{\text{SR}}(\mathbf{R}) + \mathbf{D}_{\delta}^{\text{IBS}}) \rangle,$$

$$\sigma_{\delta}^2 = \tau_{\delta}(\mathbf{E}_{\text{SR}}) (\mathbf{D}_{\delta}^{\text{SR}}(\mathbf{R}) + \mathbf{D}_{\delta}^{\text{IBS}})$$

where

$$\delta \equiv \frac{\mathbf{E} - \mathbf{E}_0}{E_0}, \quad \mathcal{H} \equiv \tilde{\eta}^T \tilde{\eta}, \quad \bar{\eta} \equiv \begin{bmatrix} \eta_{\mathbf{x}} \\ \eta'_{\mathbf{x}} \end{bmatrix}, \quad \tilde{\eta} \equiv \mathbf{A}^{-1} \bar{\eta}, \quad \mathbf{A}^{-1} = \begin{bmatrix} 1/\sqrt{\beta_{\mathbf{x}}} & \mathbf{0} \\ \alpha_{\mathbf{x}}/\sqrt{\beta_{\mathbf{x}}} & \sqrt{\beta_{\mathbf{x}}} \end{bmatrix}$$

# IBS Trade-Off



# Touschek Lifetime

Cross section (Møller scattering)  $\times$  phase space density [9]

$$\frac{1}{\tau_{1/2}} = \frac{r_e^2 c_0 N_e}{8\pi\gamma^3 \sigma_s} \frac{1}{C} \oint \frac{F\left[\left(\frac{\hat{\delta}(s)}{\gamma\sigma_{x'}(s)}\right)^2\right]}{\sigma_x(s)\sigma_z(s)\sigma_{x'}(s)\hat{\delta}(s)} ds$$

where

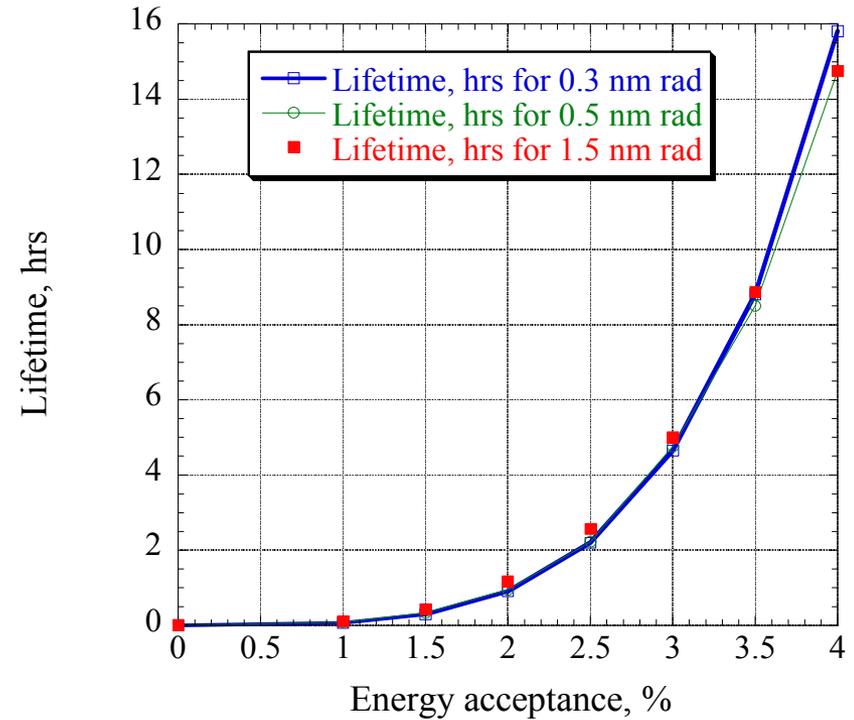
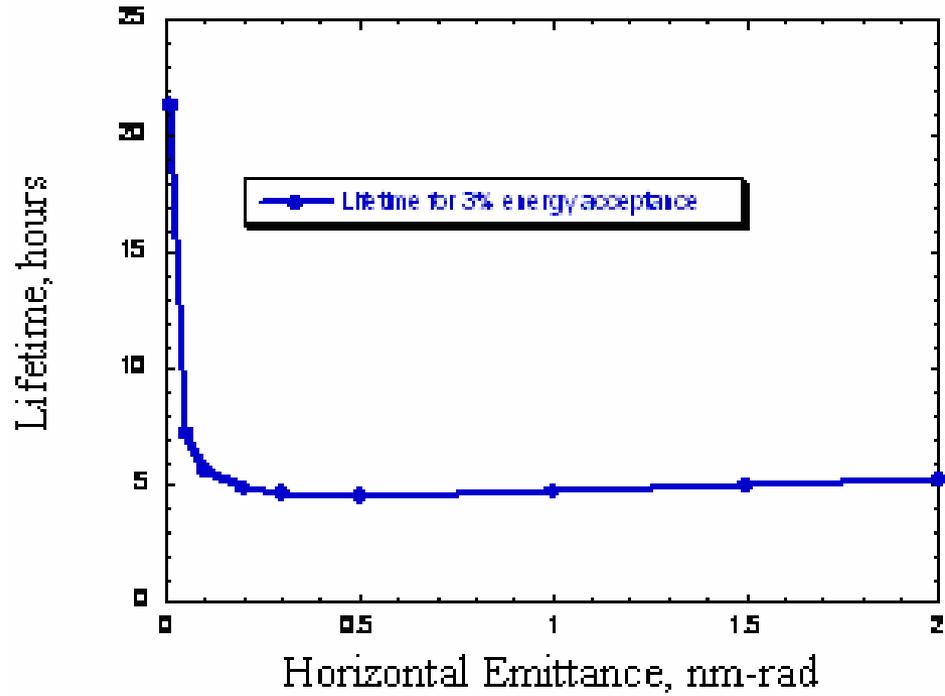
$$F(x) = \frac{1}{2} \int_0^1 \left[ \frac{2}{u} - \ln\left(\frac{1}{u}\right) - 2 \right] e^{-x/u} du$$

$r_e$  classical electron radius,  $N_e$  no of electrons/bunch,  $\sigma_s$  rms bunch length,

$C$  circumference,  $\sigma_x(s)$ ,  $\sigma_z(s)$  horizontal- and vertical rms beam size,

$\sigma_{x'}(s)$  horizontal rms beam divergence,  $\hat{\delta}(s)$  momentum acceptance.

# Touschek Life Time Trade-Offs



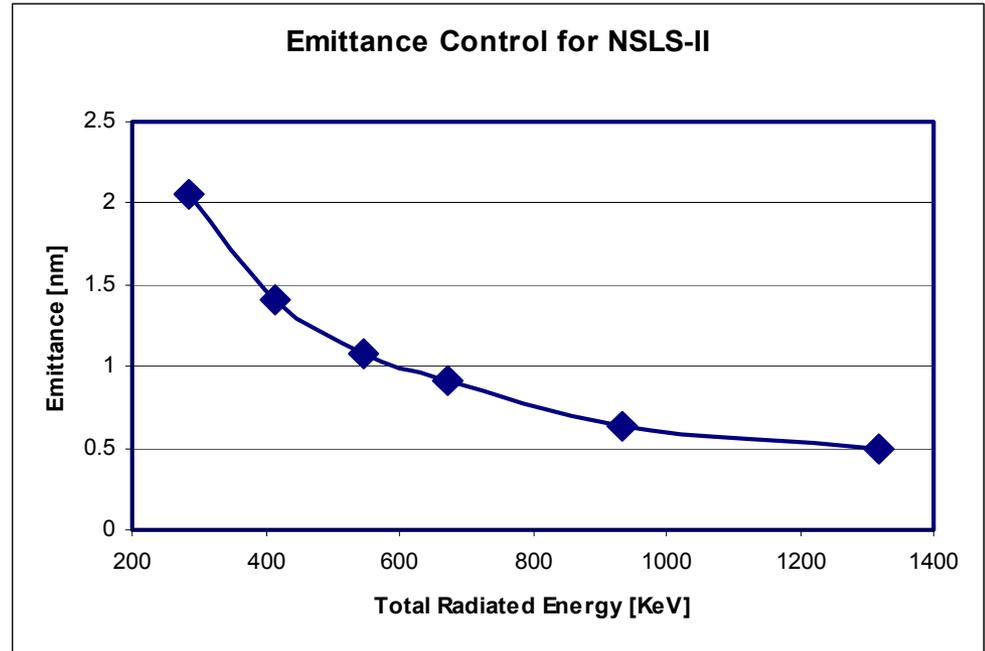
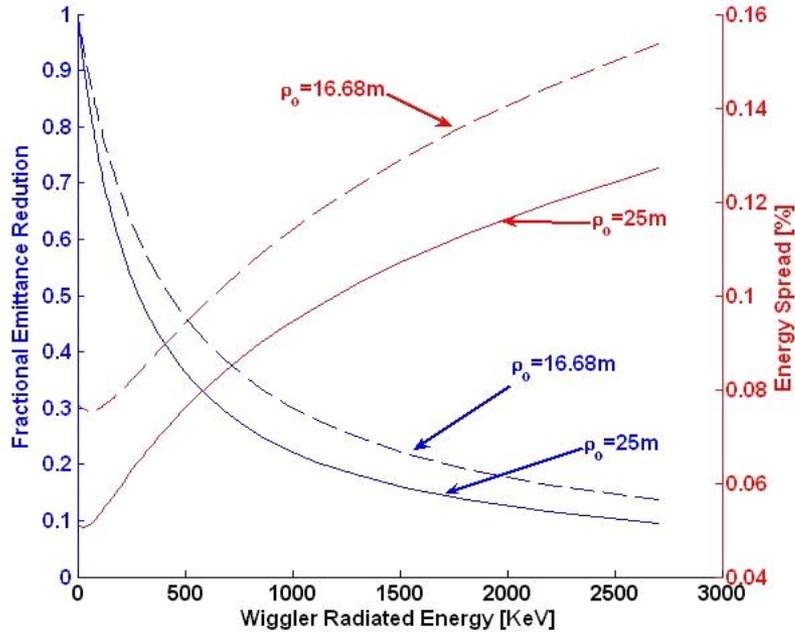
# Damping Wigglers

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The natural horizontal emittance scales with the radiated power

$$\frac{\varepsilon_w}{\varepsilon_0} \approx \frac{U_0}{U_0 + U_w}, \quad \frac{\delta_w}{\delta_0} = \sqrt{\frac{1 + \frac{8}{3\pi} \frac{B_w U_w}{B_0 U_0}}{1 + \frac{U_w}{U_0}}}$$

# Damping Wiggler Trade-Offs



# Optics Design Guidelines

The traditional approach, i.e., to first design the linear optics and then attempt to control the DA is inadequate for high performance lattices e.g. [10-11]. For a streamlined approach, the nonlinear effects must be considered from the start [12]. In particular, the following guidelines have been provided (the numbers have evolved with time) [13]:

- horizontal chromaticity per cell,  $\xi_x \leq 3.5$ ,
- horizontal peak dispersion  $0.3 \text{ m} \leq \eta_x \leq 0.5$ ,

and

	Hor and Ver Dynamic Acceptance [mm-mrad]	Hor DA [mm]	$\delta$ [%]
Bare Lattice (2.5 D.O.F.)	~25	$\pm 20$	$\pm 2.5$
“Real” Lattice (3 D.O.F.)	~20	$\pm 15$	$\pm 2.5$

# Optics Constraints

The DBAs have ~6 constraints:

- linear achromat ( $\eta_x = \eta'_x = 0$  at the entrance),
- small emittance ( $\min(\mathcal{H}) \Rightarrow (\alpha_x, \beta_x)$  fixed at the entrance),
- and symmetric ( $\alpha_{x,y} = 0$  at the center).

Similarly, the long- and short matching sections have 10 constraints:

- symmetric ( $\alpha_{x,y} = 0$  at the center),
- $\beta_{x,y}$  at the center,
- and the cell tune  $\nu_{x,y}^{\text{cell}}$ .

On the other hand, the lattice has only 8 quadrupole families.

# Generalized Higher Order Achromat

- Introduce two chromatic sextupole families and choose the cell tune for  $N$  super cells  $\mathcal{M}$  such that

$$\mathcal{M} = \mathcal{M}_1 \mathcal{M}_2 \dots \mathcal{M}_N, \quad \mathcal{M}_k = \mathcal{A}^{-1} \mathbf{e}^{i h \cdot} \mathcal{R} \mathcal{A}, \quad \mathcal{R}^N = \begin{bmatrix} I & 0 \\ 0 & \pm I \end{bmatrix}$$

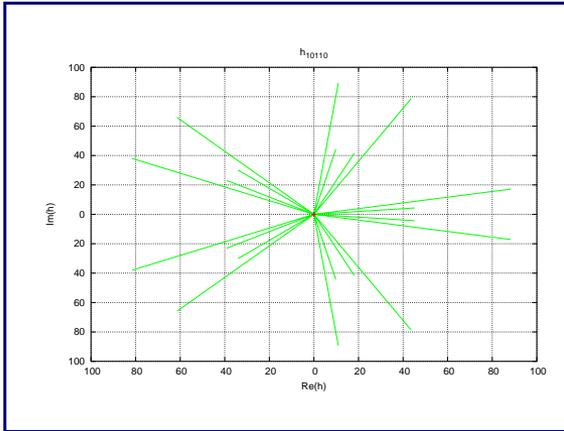
In particular, so that resonances up to 4th order

$$n_x \nu_x + n_y \nu_y = n, \quad |n_x| + |n_y| \leq 4$$

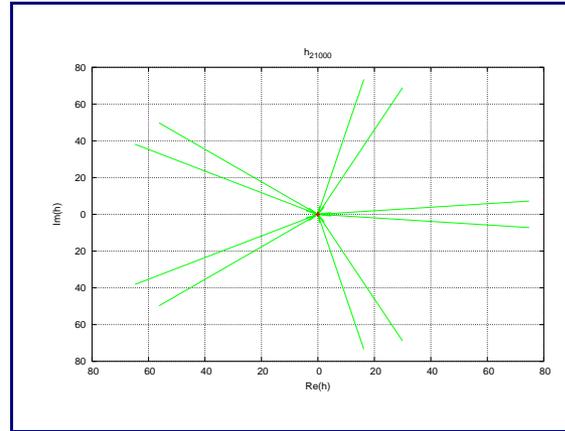
are cancelled (by symmetry):

- Control the residual amplitude dependent tune shift and free up the choice of working point by adding geometric sextupoles [SLS].
- Control the residual nonlinear chromaticity by adding chromatic multipole families as needed.
- Optimize dynamic- and momentum aperture (from tracking) by joint minimization of the driving terms and variation of the cell tune.

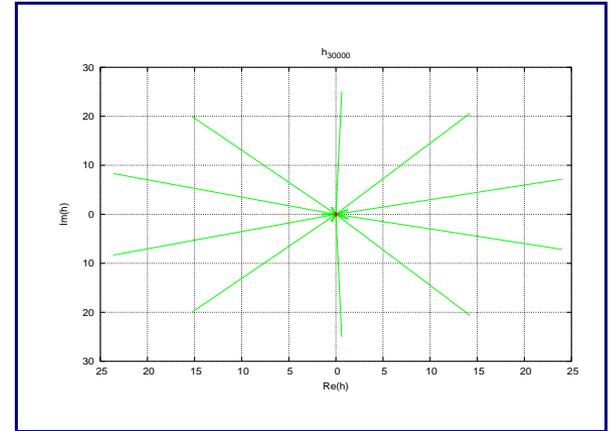
# A 5-Cell Second Order Achromat (2 chrom families)



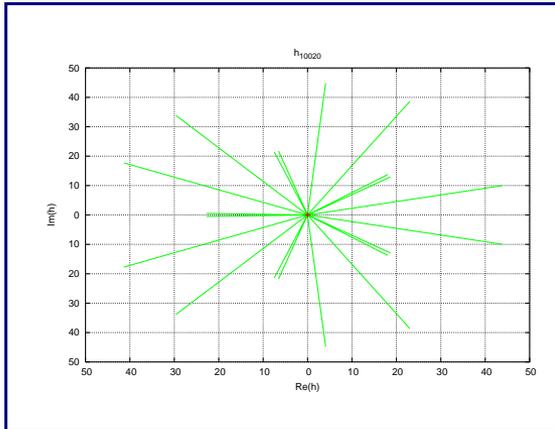
$h_{10110}$



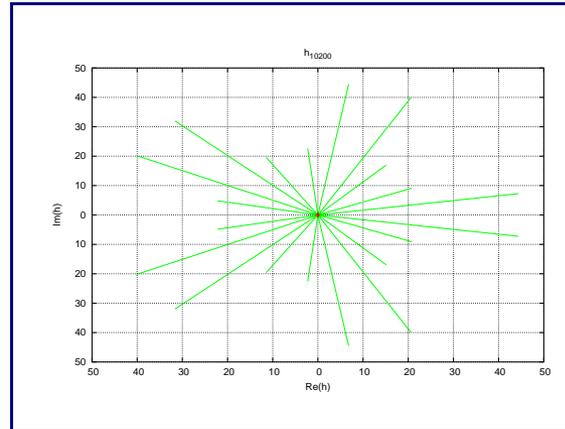
$h_{21000}$



$h_{30000}$

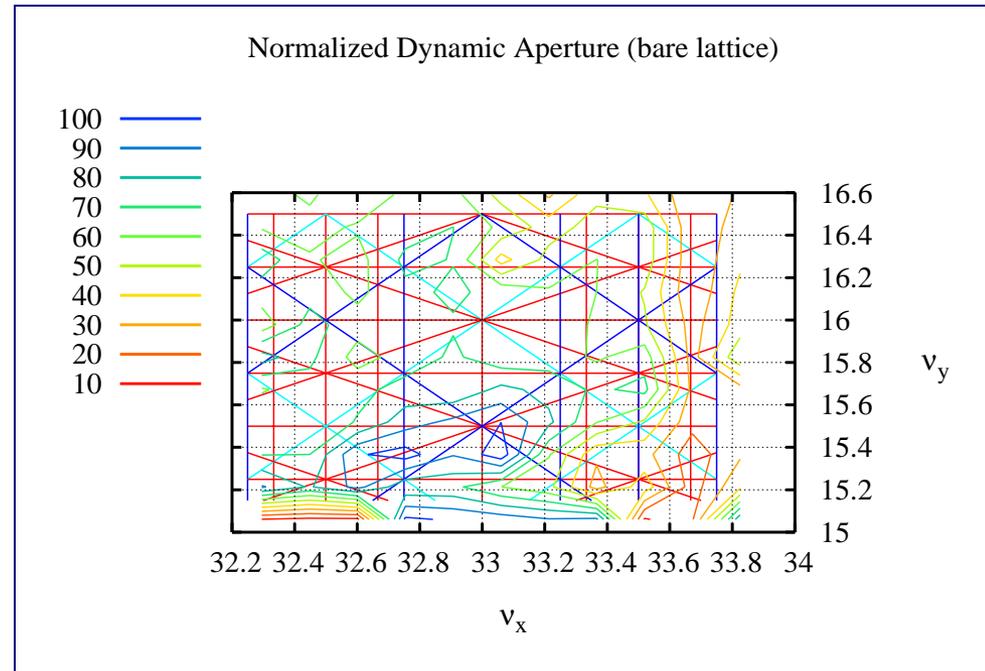
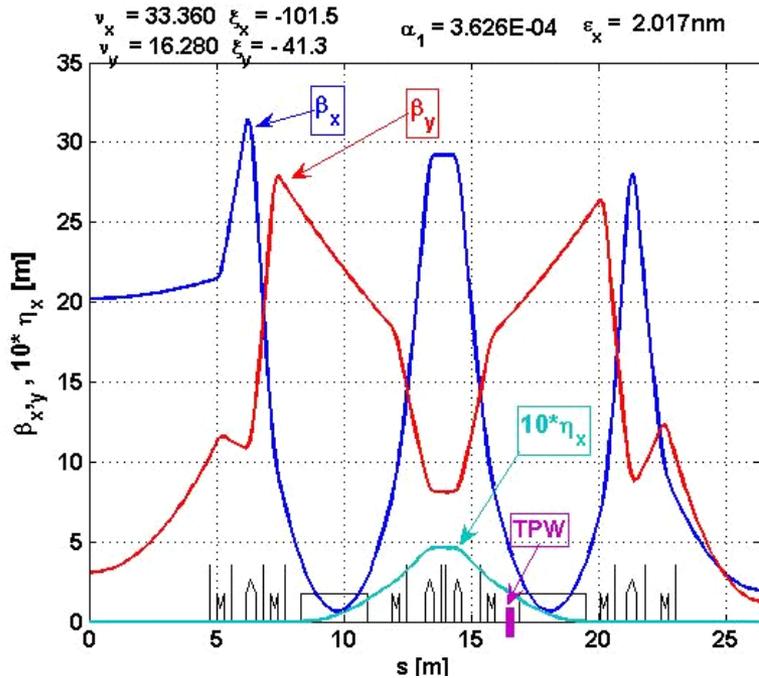


$h_{10020}$



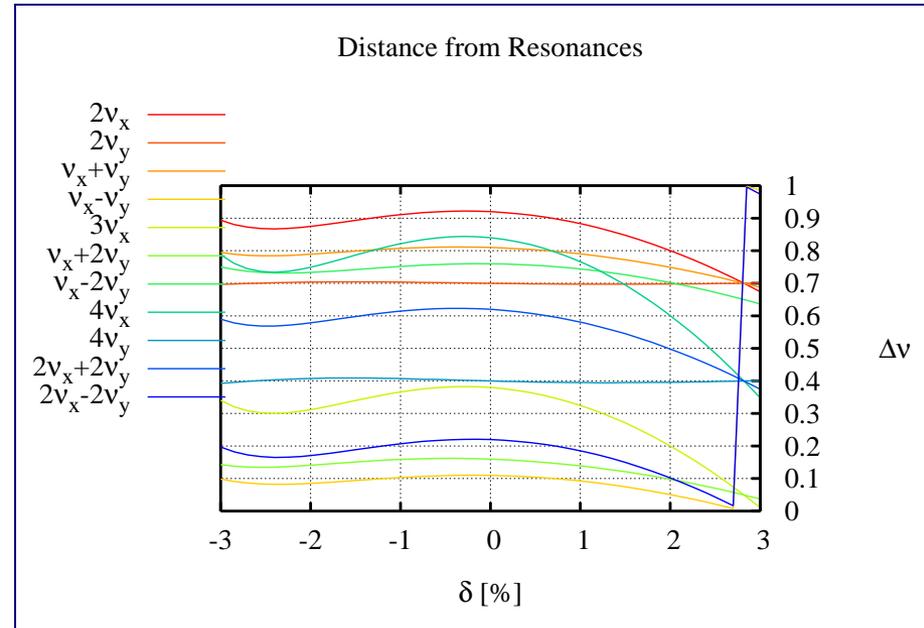
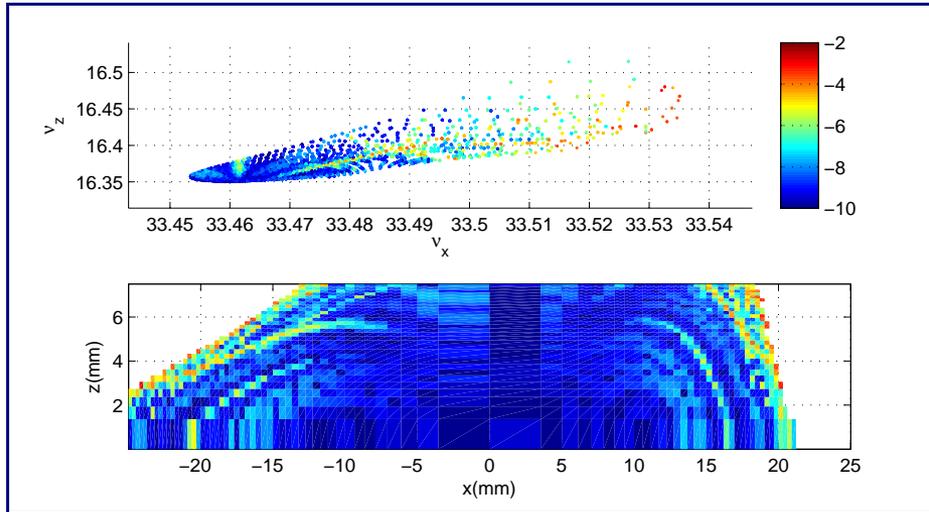
$h_{10200}$

# Linear Optics and Tune Scan

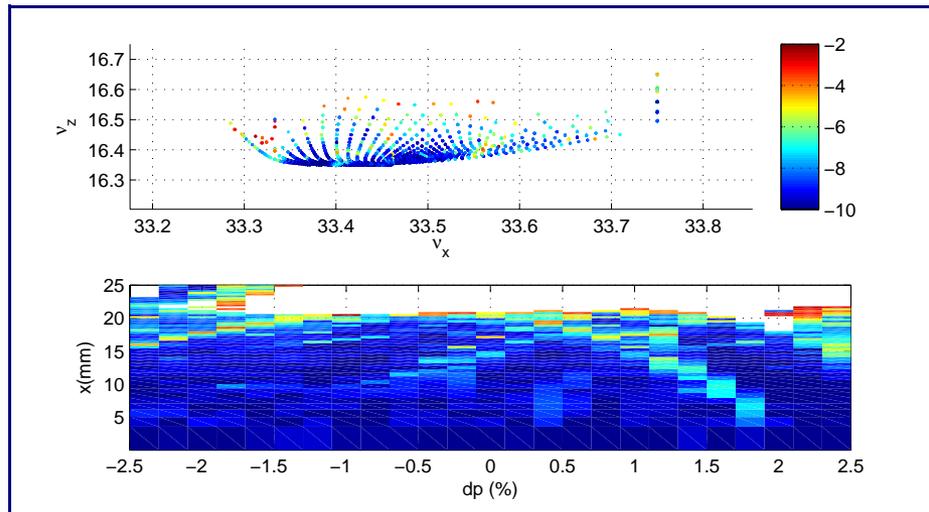


- An  $11 \times 11$  grid of working points is obtained that meets optics requirements.
- For each working point, the driving terms are minimized and a weighted average of the dynamic- and momentum aperture ( $DA / \sqrt{\beta_x \beta_y}$ ) is computed by tracking.

# Frequency Map and Resonance Avoidance



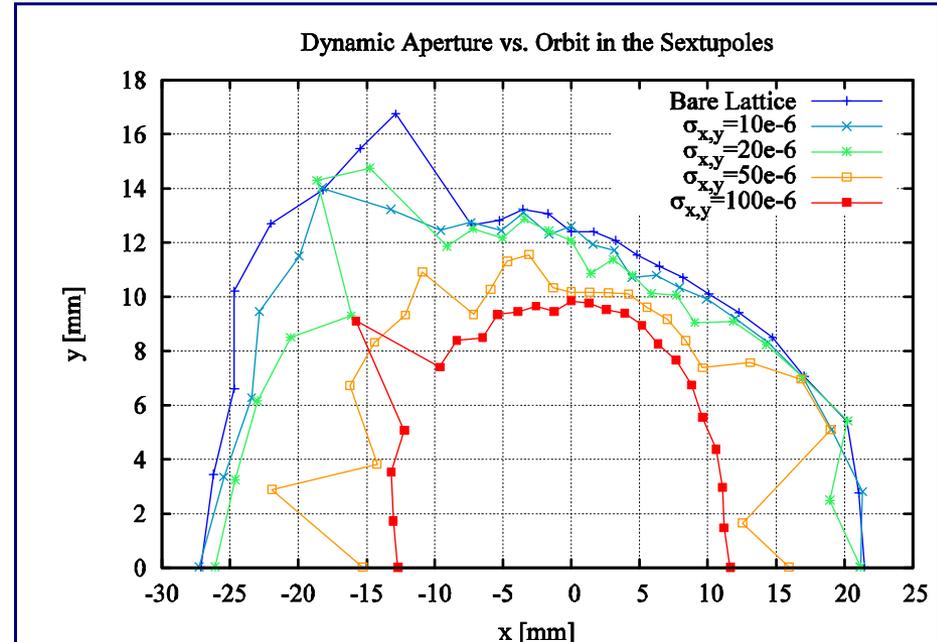
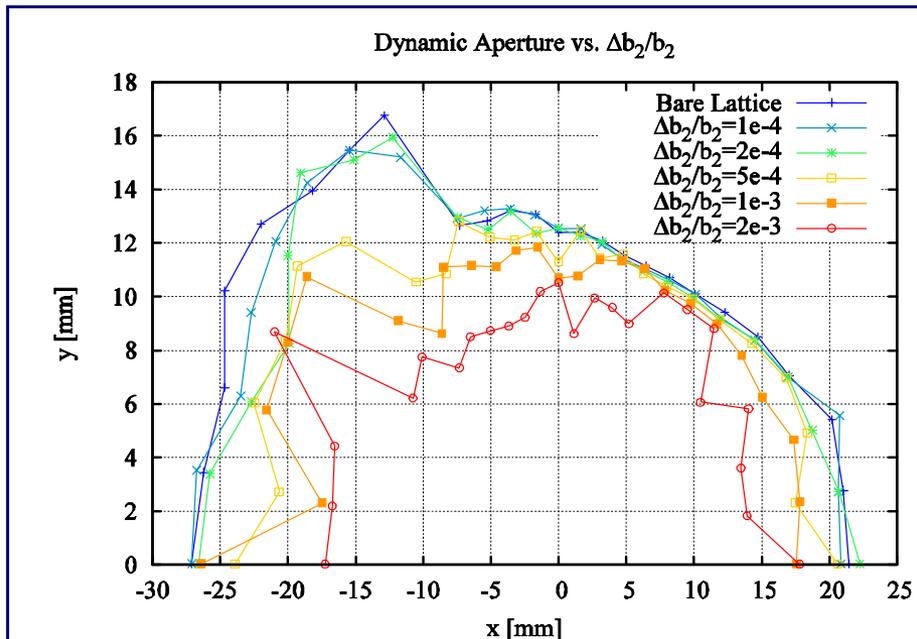
without DWs.



# Optics Tolerances

## Estimated tolerances

Parameter	$\Delta b_2/b_2$	$(\Delta\beta_{x,y}/\beta_{x,y})_{\text{rms}}$	$(\Delta v_{x,y})_{\text{rms}}$	$(\Delta x_{\text{cod}}, \Delta y_{\text{cod}})_{\text{rms}}$
Tolerance	$\sim 5 \times 10^{-4}$	$\sim (2\%, 3\%)$	$\sim (0.003, 0.002)$	$\sim (50, 50) \mu\text{m}$



# Impact of Insertion Devices

The averaged Hamiltonian is (planar)

$$\langle H \rangle_{\lambda_w} = \frac{p_x^2 + p_y^2}{2(1 + \delta)} + \left( \frac{B_w}{B\rho} \right)^2 \frac{\cosh^2(k_y y)}{4k_z^2(1 + \delta)} - \delta + \mathcal{O}(p_{x,y})^4, \quad k_y = k_z = \frac{2\pi}{\lambda_w}$$

To leading order one obtains

$$\Delta v_y = \frac{1}{8\pi} \left( \frac{B_w}{B\rho} \right)^2 \langle \beta_y \rangle L_w, \quad \frac{\partial v_y}{\partial J_y} = \frac{\pi}{4} \left( \frac{B_w}{B\rho} \right)^2 \frac{\langle \beta_y^2 \rangle L_w}{\lambda_w^2}$$

Since  $\beta(\mathbf{s}) = \beta_0 [1 + (\mathbf{s}/\beta_0)^2]$ , optimum beta for min impact is:

stay clear  $\Rightarrow \beta_0 = L/2$ , linear optics  $\Rightarrow \beta_0 = L/2^4\sqrt{3}$ ,

nonlinear dynamics  $\Rightarrow \beta_0 = L/2^4\sqrt{5}$ .

# Conclusions

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- The “chromaticity wall” has been avoided by using damping wigglers. Furthermore, these turned out to be useful high-flux X-Ray sources.
- The emittance can be reduced as the facility evolves.
- The nonlinear effects are taken into account for the optics design. In particular, by providing guidelines for chromaticity per cell and peak dispersion.
- The dynamic- and momentum aperture are improved by implementing a generalized higher order achromat. It is optimized by a joint optimization of the driving terms and working point.
- The ultimate-low emittance limit can be reached by this approach. It is a matter of power consumption and circumference.

# References

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- [10] G. Mülhaupt et al “Status of the Swiss Light Source Project SLS” p. 685-687 EPAC96.
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- [12] J. Bengtsson et al “Increasing the Energy Acceptance of High Brightness Synchrotron Light Storage Rings” NIM, A404 (1997), p 237-247.
- [13] NSLS-II Preliminary Design Report (2007).
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# Back-up Slides

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# Damping Wigglers

The natural horizontal emittance scales with the radiated power

$$\frac{\varepsilon_w}{\varepsilon_0} = \frac{1+f}{1+\frac{U_w}{U_0}} \approx \frac{U_0}{U_0+U_w}, \quad \frac{\delta_w}{\delta_0} = \sqrt{\frac{1+\frac{8}{3\pi}\frac{B_w U_w}{B_0 U_0}}{1+\frac{U_w}{U_0}}}, \quad \frac{U_w}{U_0} = \frac{L_w}{4\pi\rho_0} \left(\frac{B_w}{B_0}\right)^2$$

where

$$f \cong \frac{2C_q\gamma^2 L_w \rho_0}{3\pi^2 \varepsilon_0 \rho_w^3} \left[ \frac{1}{5} \left(\frac{K_w}{\gamma}\right)^2 \langle \beta_x \rangle + \frac{\eta_{x0}^2}{\beta_{x0}} + \beta_{x0} \eta'_{x0}{}^2 \right], \quad \frac{K_w}{\gamma} = \frac{\lambda_w}{2\pi\rho_w}, \quad C_q = 3.8 \times 10^{-13},$$

$$\beta_x(\mathbf{s}) = \beta_{x0} \left[ 1 + \left(\frac{\mathbf{s}}{\beta_{x0}}\right)^2 \right], \quad \eta_x(\mathbf{s}) = \frac{1}{\rho_w} \left(\frac{\lambda_w}{2\pi}\right)^2 \left( 1 - \cos\left(\frac{2\pi\mathbf{s}}{\lambda_w}\right) \right) + \eta_{x0} + \eta'_{x0} \mathbf{s}$$

# Control of Optics

## Control of linear optics perturbation from IDs:

- optics response matrix

$$\left[ \frac{\Delta\beta_i}{\beta_i}, \dots, \Delta\mu_j, \dots, \Delta v_x, \Delta v_y \right]^T = \mathbf{T}(\beta, \mu) [\Delta\mathbf{b}_{2,1}, \dots, \Delta\mathbf{b}_{2,N_Q}]^T$$

## Control of vertical beam size:

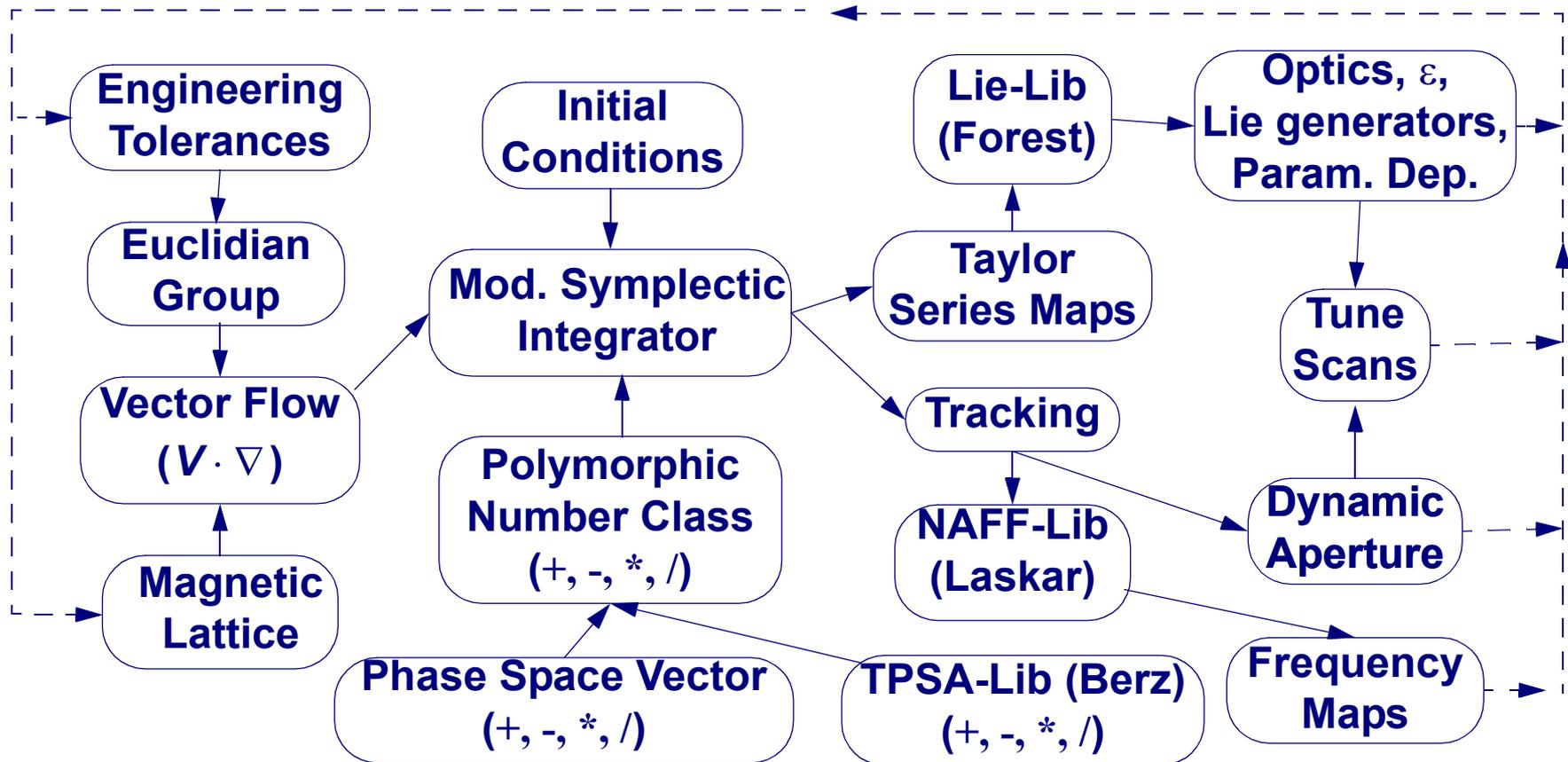
- beam response matrix

$$\left[ \frac{\partial \mathbf{x}_i}{\partial \mathbf{p}_{y,k}}, \dots, \frac{\partial \mathbf{y}_i}{\partial \mathbf{p}_{x,k}}, \dots, \Delta\eta_{y,i}, \dots \right]^T = \mathbf{U}(\beta, \mu) [\Delta\mathbf{a}_{2,1}, \dots, \Delta\mathbf{a}_{2,N_{SQ}}]^T$$

- Include dispersion wave, if needed [14].

Invert  $\mathbf{T}$ ,  $\mathbf{U}$  by SVD, compute, and apply the corrections (i.e., like orbit correction).

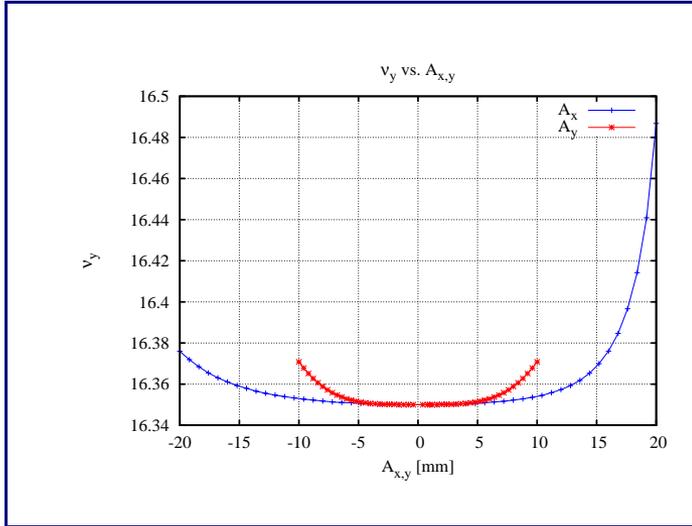
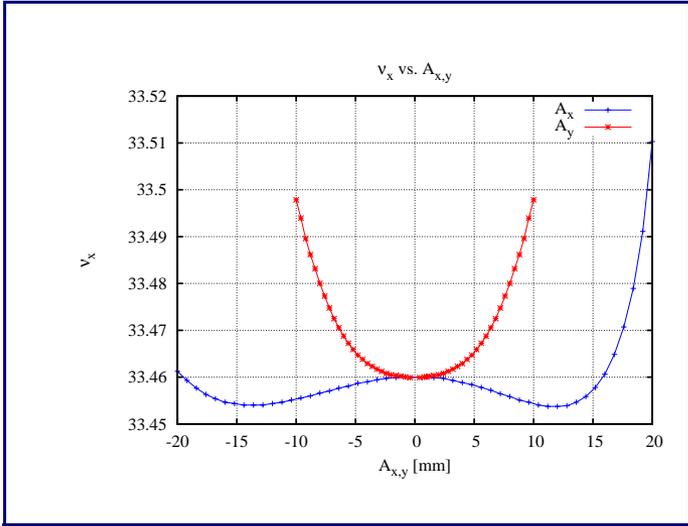
# The Polymorphic Tracking Code (PTC)



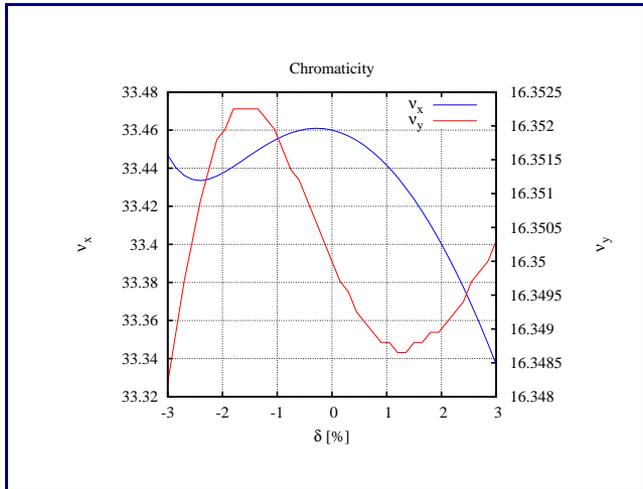
# A 10-Cell Third Order Achromat

Cell	$\square_x$	$\square_y$	$\square_x$	$2\square_x$	$3\square_x$	$2\square_y$	$\square_x-2\square_y$	$\square_x+2\square_y$	$4\square_x$	$4\square_y$	$2\square_x-2\square_y$	$2\square_x+2\square_y$
1	2.200	1.050	2.20	4.40	6.60	2.10	0.10	4.30	8.80	4.20	2.30	6.50
2	4.400	2.100	4.40	8.80	13.20	4.20	0.20	8.60	17.60	8.40	4.60	13.00
3	6.600	3.150	6.60	13.20	19.80	6.30	0.30	12.90	26.40	12.60	6.90	19.50
4	8.800	4.200	8.80	17.60	26.40	8.40	0.40	17.20	35.20	16.80	9.20	26.00
5	11.000	5.250	11.00	22.00	33.00	10.50	0.50	21.50	44.00	21.00	11.50	32.50
6	13.200	6.300	13.20	26.40	39.60	12.60	0.60	25.80	52.80	25.20	13.80	39.00
7	15.400	7.350	15.40	30.80	46.20	14.70	0.70	30.10	61.60	29.40	16.10	45.50
8	17.600	8.400	17.60	35.20	52.80	16.80	0.80	34.40	70.40	33.60	18.40	52.00
9	19.800	9.450	19.80	39.60	59.40	18.90	0.90	38.70	79.20	37.80	20.70	58.50
10	22.000	10.500	22.00	44.00	66.00	21.00	1.00	43.00	88.00	42.00	23.00	65.00

# Tune Footprint



without DWs.



# Frequency Map and Resonance Avoidance (w DWs)

